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Experimental study of the liquid velocity and turbulence in a large-scale air-water counter-current bubble column

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Abstract

Measuring the local liquid velocity and turbulence in large-scale bubble columns with optical methods is complex and usually limited to low gas holdups in thin geometries. Comprehensive datasets in large bubble columns are therefore seldom published. Since the importance of Computational Fluid Dynamics (*CFD*) is increasing for multiphase applications, such data is also important for validating models for dispersed bubbly flows. In the present work the liquid velocity and turbulence in a pilot-scale bubble column is studied and a *CFD* validation database is generated by completing previous measurements of the gas void fractions and bubble sizes. For this purpose, we used a Particle Shadowgraph Velocimetry (*PSV*) technique that was intentionally designed to study the fluid dynamics in large-scale facilities. The measurements were realized in the 5.3 m high and 0.24 m diameter counter-current bubble column at Politecnico di Milano. The superficial gas velocity ranged from 0.37 to 1.85 cm/s, the counter current superficial liquid velocity from 0 to 9.2 cm/s. All operation points are in the so-called pseudo-homogeneous flow regime, in which the integral gas holdup (ranging from 1.02 to 7.55 %) increases linear with the superficial gas velocity but an inhomogeneous flow is present. The dominant frequencies of the bubbly flow, shear rates, and turbulence levels are increasing with increasing superficial gas velocity. With increasing superficial liquid velocities, the dominant frequencies are decreasing, the averaged liquid velocities are shifted downwards, but the overall turbulence levels remain constant. In order to investigate the smaller scales at which the bubble-induced turbulence is expected, a filtering process is proposed. As a result, the filtered turbulence levels of all operation points fall on a linear trend line when plotted over the local void fraction, which is the same result obtained in other studies in small, homogenous tabletop columns. The now available database for *CFD* validation contains the averaged liquid velocities, basic turbulence information, local void fractions, and the bubble sizes at two different heights. The data will be in particular useful to

validate the capabilities of models to upscale bubbly flows from tabletop to the pilot-scale bubble columns.

Keywords

Bubbly flows, particle-tracking velocimetry, multiphase turbulence, pilot-scale bubble columns, CFD database

1 Introduction

Bubbly flows are characterized by the strong connection of three main parameters: (a) liquid velocity, (b) gas fraction, and (c) bubble size distribution. Specifically, the fluid dynamics in bubble columns are subject to this connection since the bubbles drive the liquid flow, which in reverse influence the rising characteristic and break-up/coalescence of the bubbles. In particular, the local-scales (i.e. break-up/coalescence, force balance, etc.) are strongly coupled to the integral-scale (i.e. gas-holdup, flow regime, etc.). Consequently, all three parameters need to be considered in order to understand the dynamics of bubbly flows and to improve the modeling strategies at the different scales.

Usually for the three parameters mentioned above, different measuring techniques are used. With probes, the local gas volume fraction is relatively simple accessible (Schleicher et al. 2008). Measuring the Bubble Size Distribution (*BSD*), however, is more complicated. Nevertheless, evaluating bubble sizes manually from pictures is a simple but time-consuming method with which reasonable results can be obtained in optical assessable setups (e.g. Besagni & Inzoli (2016a)). The methods for measuring the liquid velocity in bubbly flows are manifold and adapted from single-phase flows. The most frequently used methods are Particle Image Velocimetry (*PIV*) (e.g. (Hessenkemper & Ziegenhein 2018)), Laser Doppler Anemometry (*LDA*) (e.g. (Hosokawa & Tomiyama 2013)), and Hot Film Anemometry (*HFA*) (e.g. (Rensen et al. 2005)). In the large group of *PIV* methods with (Deen et al. 2002) and without (Ziegenhein et al. 2016a) laser illumination falls the Particle Tracking Velocimetry (*PTV*) method, which is used in the present work. When no lasers are used for *PIV* measurements, usually a background light is applied so that the shadows of particles are recorded, which is called Particle Shadowgraph Velocimetry (*PSV*) (Hessenkemper & Ziegenhein 2018). *PSV* methods are not common, but they have some advantages in bubbly flows.

One advantage of *PSV* methods is the possibility of a permanent light source so that no extra trigger is needed, which simplifies the setup distinctly. However, more importantly for a field measurement is that background lights has very little safety requirements compared to a laser. This advantage is often vital to perform measurements at large test facilities built up in a non-laser lab environment. From our experience, another advantage of background light is that they can be used at higher volume fractions in bubbly flows. A two-dimensional laser light sheet is distorted at the bubble surface so that on one hand, large shadows behind the bubbles occur and on the other hand, particles are illuminated before and behind the supposed two-dimensional measurement plane due to reflections. A technical advantage is that no fluorescence tracers are needed. Particles with a fluorescent pigment coated on the particle surface contaminate the bubbly flow distinctly since the pigment is usually hydrophobic. Particles with an encapsulated pigment are expensive (considering a fluid volume of around 200 liter), often limited to specific sizes or are not neutrally buoyant. However, the disadvantage of background light is the volume illumination and the connected problem of selecting particles on a two-dimensional plane.

41 This is realized in the present work by using a thin depth of field and selecting sharp
42 particles in the post-processing.

43 By using *PTV* instead of *PIV*, further problems are avoided. First, masking bubbles
44 (Jakobsen et al. 1996) (Pang & Wei 2013) in the post processing or even recording the
45 bubbles in a separate step (Delnoij et al. 2000) (Bröder & Sommerfeld 2007) is not
46 necessary. A second advantage of *PTV* is that a lower tracer-particle density can be used.
47 Because the velocity is measured in gaps of rising bubble swarms in the present study, a
48 relatively high spatial resolution – i.e. small interrogation areas – for *PIV* would be needed.
49 Such a high spatial resolution requires a high seeding, which blocks the light and causes a
50 distinct contamination of the bubbles with tracers. Another problem with *PIV* in dense
51 bubbly flows is that neighboring interrogation areas are masked due to the presence of the
52 bubbles. Since robust single-phase flow *PIV* algorithms use neighboring interrogation areas
53 for iteration or validation, those would be not applicable. With the chosen particle seeding
54 and spatial resolution, *PTV* can handle higher void fractions. Nevertheless, *PIV* methods
55 work well in bubble free zones (Murgan et al. 2017), discrete gas sparger setups (Lindken
56 & Merzkirch 2002) (Rzehak et al. 2017) or low void fractions (Delnoij et al. 1999). Using
57 techniques that are more advanced, like the *LIF-PLV* technique described by Bröder and
58 Sommerfeld (2002), dense bubbly flows can be investigated with *PIV*. Certainly, all *PTV* and
59 *PIV* techniques are behind one-point measurements like *LDA* (Mudde et al. 2009) and *HFA*
60 (Mercado et al. 2012) in terms of maximum void fraction. However, these measuring
61 techniques have also some drawback and the phase discrimination is not trivial.

62 Due to the described advantages, *PTV* combined with a shadowgraph setup, called from
63 here on Particle Shadowgraph Tracking Velocimetry (*PSTV*), was used in the present study.
64 The measurements were conducted at the counter-current bubble column located at the
65 Department of Energy of Politecnico di Milano (Besagni & Inzoli 2016a) (Besagni et al.
66 2017). The 5.3 m high and 0.24 m diameter column was developed concerning the well-
67 known scaling-up criteria “*large-diameter*” and the “*large-scale*” concepts, discussed in the
68 pioneering study of (Wilkinson et al. 1992) and, more recently by (Besagni et al. 2017a),
69 where the “*large-diameter*” concept has been related to the Rayleigh–Taylor instabilities
70 (Kitscha, & Kocamustafaogullarim, 1989). The gas was distributed in the column at the
71 bottom via a spider-sparger that is typically used in industrial applications. The dimensions
72 of the bubble column are therefore in the range of a pilot-scale facility that is used to scale-
73 up results from laboratory-scale to the final, industrial scale (Shaikh & Al-Dahhan, 2013). In
74 addition, the facility is equipped with a water pump so that the liquid can be recirculated in
75 an external loop. Gas superficial velocities were used in the range of $U_G = 0.37\text{--}1.85$ cm/s,
76 the liquid was recirculated at several superficial liquid velocity from $U_L = 0.0$ cm to -9.2
77 cm/s, where 0.0 cm/s refers to the batch mode (i.e. gas is dispersed in a standing liquid
78 column). All experiments were performed in the boundaries of the pseudo-homogeneous
79 flow regime, as classified by Besagni et al. (2016a, b) (2018). The gas holdup, in the above-
80 mentioned conditions, was ranging from 1.02 to 7.55 %.

81 From the measurements, the transient as well as time-averaged liquid velocities are
82 determined. The components of the Reynolds stress tensor are distinctly influenced by a
83 bubble plume found in the column. Therefore, a filtering process is proposed with which
84 the smaller-scales can be investigated. Comparing the filtered results to other
85 measurements in small-scale bubble columns, surprising similarities are found, which
86 indicate a similarity of the bubble induced turbulence. Bubble induced turbulence in
87 general is an important effect in order to model for example coalescence and break-up
88 (Liao & Lucas 2009) or mixing (Alm eras et al. 2015) correctly. In the recent years, the
89 turbulence in bubbly flows is subject to many publications, from single bubble
90 investigations (Liu et al. 2005) over bubble columns (Julia et al. 2007) to two-phase pipe
91 flows (Hosokawa & Tomiyama 2013). With increasing computational power, the topic is
92 also in the focus of Direct Numerical Simulations (*DNS*) (Ma et al. 2017) and Large Eddy
93 Simulations (*LES*) (Fraga et al. 2016). Several models exist with specific aims, for example
94 the (Reynolds Averaged Navier Stokes) RANS modeling is reviewed by Rzehak & Krepper
95 (2013a) and a model to match the often reported slope deviation in the energy spectra is
96 proposed by Riboux et al. (2013). In the present work, we evaluate the change of the
97 bubble induced turbulent kinetic energy with the (local) void fraction with a filtering
98 process. Further, the findings are compared to the experiments of Julia et al. (2007) as well
99 as Lance & Bataille (1991) and to the linear hypothesis of Nigmatulin (1979).

100 Such velocity measurements at pilot-plant scale are rarely reported in the literature, in
101 particular for counter-current bubble columns. The present measurements complete
102 previous gas volume fraction and bubble size measurements (Besagni & Inzoli 2016a) to
103 provide a comprehensive *CFD* validation database. Such data that covers the continuous
104 and dispersed phase properties resolved locally at different position in the facility are vital
105 for advancing the model development (Lucas et al. 2016).

106 2 Experimental setup and methods

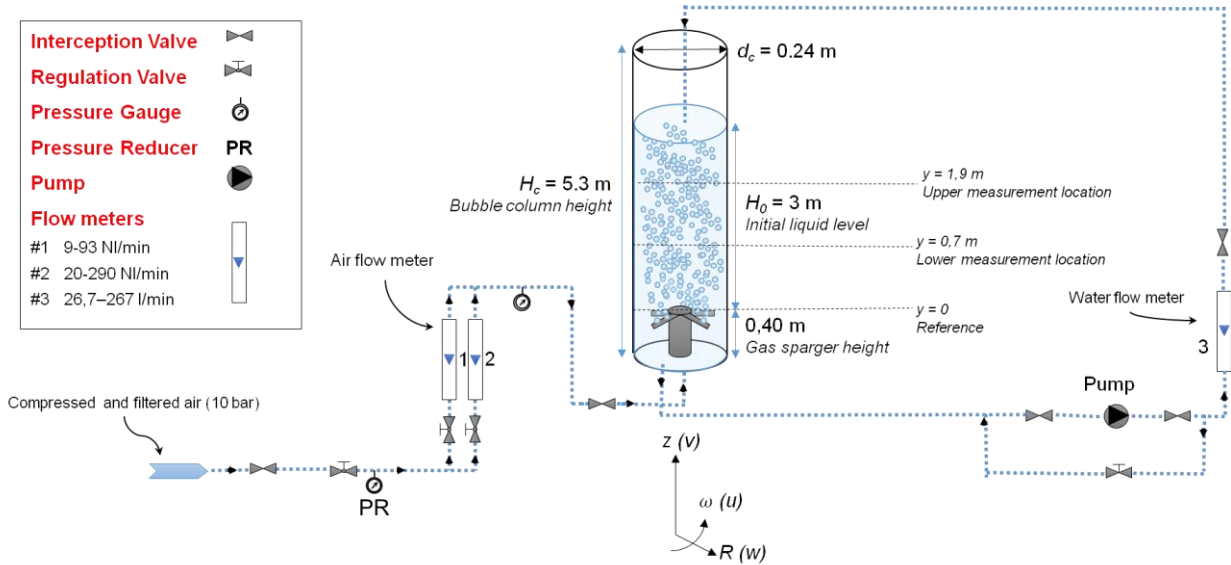
107 This section aims to present the experimental setup and to provide the needed background
108 to better interpret the experimental data. First, the experimental setup is briefly described;
109 second, the *PTV* method is introduced. The reader may refer to Appendix A for a discussion
110 concerning the prevailing flow regimes, the local and the global flow properties in the
111 conditions examined in this paper are briefly discussed. In addition, a discussion of the flow
112 regimes in large-scale bubble columns can be found in our recent review paper (Besagni et
113 al. 2018).

114 2.1 Experimental setup

115 The experimental facility (Figure 1) is a non-pressurized vertical pipe made of Plexiglas. A
116 pressure reducer controls the pressure upstream of the rotameters (1) and (2), which are
117 used to measure the gas flowrate (E5-2600/h, manufactured by ASA, Italy). The accuracy of
118 the measured integral gas flow rate is $\pm 2\%$ with a repeatability error of under $\pm 0.25\%$. A

119 pump, which is controlled by a bypass valve, provides water recirculation and a rotameter
 120 (3) measures the liquid flowrate (G6-3100/39, manufactured by ASA, Italy). The accuracy
 121 of the measured liquid flow rate is $\pm 1.5\%$ with a repeatability error of under $\pm 0.5\%$. The
 122 air distributor is a spider-gas sparger, which is similar to the distributors used in industrial
 123 application. The spider sparger, shown in Figure 2, has six arms (120 mm diameter, made
 124 of stainless steel) tubes soldered to the central cylinder of the sparger. The angle between
 125 the different tubes is 60° . There are six holes (hole-diameters in the range of 2–4 mm,
 126 Figure 2c and Figure 2d) located on the side of each arm facing upward; these holes are
 127 distributed as shown in Figure 2d, with the hole diameter increasing toward the column
 128 wall. In addition, there are four holes, located on the header of the gas sparger, located as is
 129 Figure 2d. A porous plate has been included in the lower part of the gas sparger, to ensure a
 130 uniform liquid velocity profile and avoid preferential path induced by the water outlet.
 131 Owing to the gas sparger opening, the produced bubble size distribution (*BSD*) is
 132 polydispersed (Figure 29, in Appendix A). Filtered air and filtered, deionized water were
 133 used; during the experiments, the air and water temperatures were maintained constant at
 134 room temperature (22°C). The values of the gas density, which were used to compute the
 135 superficial gas velocity, U_G , are based upon the operating conditions existing at the column
 136 midpoint (Reily et al. 1994) and are computed by using the ideal gas law.

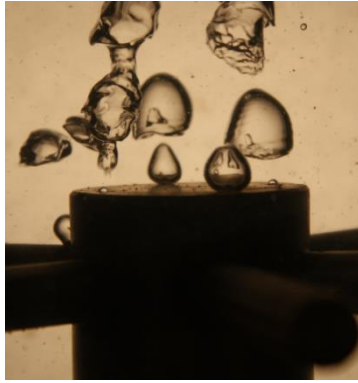
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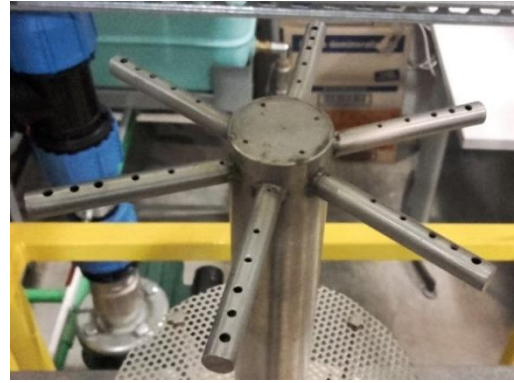
Figure 1 The experimental setup



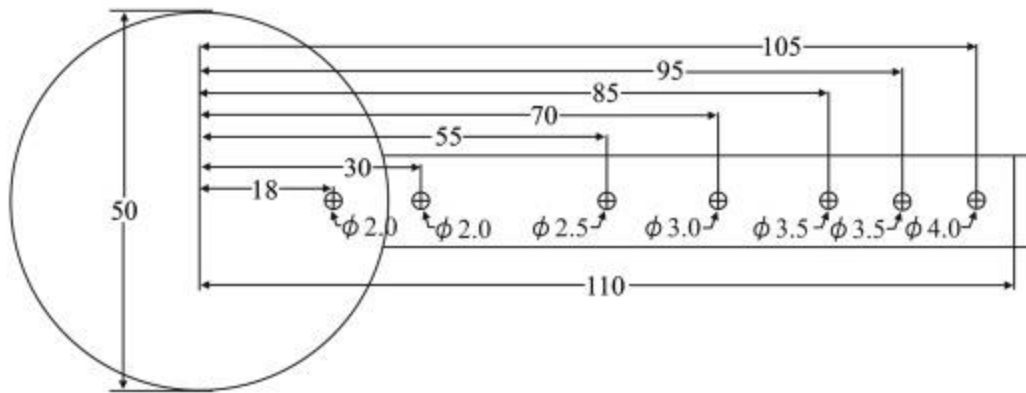
(a) Bubbles at the gas sparger at low sup. gas velocity



(b) Spider gas sparger



(c) View from top

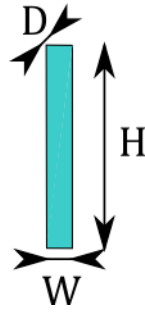
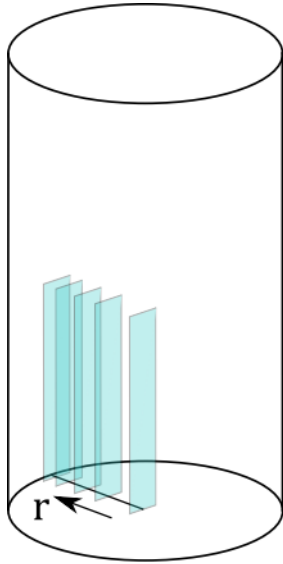


(d) Spider gas sparger: distribution and diameter of the holes on one of the arms (measurements in mm)

140 Figure 2 The gas sparger (spider-sparger) – Besagni et al. (2017) and Besagni and Inzoli,
 141 (2016a)

142 2.2 Measurement setup

143 The liquid velocity measurements were realized at the two measuring heights where the
 144 previous optical probes measurements took place (see Besagni and Inzoli (2016a)), namely
 145 at $h= 1.9$ m and 0.7 m above the gas-sparger. As explained in the introduction, the
 146 measuring concept is a shadowgraph technique with a backlight, which was an air-cooled
 147 400W halogen lamp. To obtain a quasi-two-dimensional measuring plane, the depth of field
 148 was adjusted to 2 mm by using a Samyang lens with an aperture of 2.0, a focal length of
 149 135, and a focus distance of 1300 mm. The optical setup with the Q-VIT high-speed camera
 150 from AOS Technologies AG was placed on a linear unit (± 0.020 mm on 300 mm) to move it
 151 stepwise along the column radius. With this method, we obtained 11 measuring planes of
 152 6x25.3 mm (Width x Height) with a resolution of 397x1686 pixels along the radial
 153 coordinate as shown in Figure 3. The positions of the planes were chosen so that near the
 154 wall, where higher gradients of the time averaged liquid velocities are expected, a higher
 155 radial resolution is obtained.



W = 6 mm, H = 25.3 mm, D = 2 mm,
 Resolution = 0.0115 mm/Pixel,
 Measuring time per plane = 1000 s

Position	Radial coordinate, r [m]
1	0.119
2	0.116
3	0.113
4	0.110
5	0.100
6	0.090
7	0.080
8	0.060
9	0.040
10	0.020
11	0.000

156 Figure 3 Scheme of the measuring concept.

157 In order to minimize optical distortions due to the round shape of the bubble column, a box
 158 filled with water was placed around the bubble column. Since the water in the box and the
 159 Plexiglas® of the bubble column have almost the same refraction index, it is assumed that
 160 no optical distortion due to round shape of the bubble column is present. This concept has
 161 been verified in a previous study by Besagni and Inzoli (2016b), in an annular gap bubble
 162 column, to whom the reader may refer. In addition, this is a common technique for PIV
 163 measurements in round shapes, e.g. in pipes (van Doorne & Westerweel 2007). The linear
 164 unit was moved perpendicular to the box, the radial positions in the bubble column were
 165 calculated with the refraction index of water. The measurements were calibrated by using a
 166 microscope calibration plate with an accuracy of 10^{-4} mm. In the following, the horizontal
 167 velocity in the planes is referred as angular velocity. Due to the narrow measuring plane of
 168 6 mm, the off-set error to an circle for the measuring position at a radial coordinate of 0.02
 169 m would be 0.500 mm. Therefore, this geometrical error is neglected in the following.

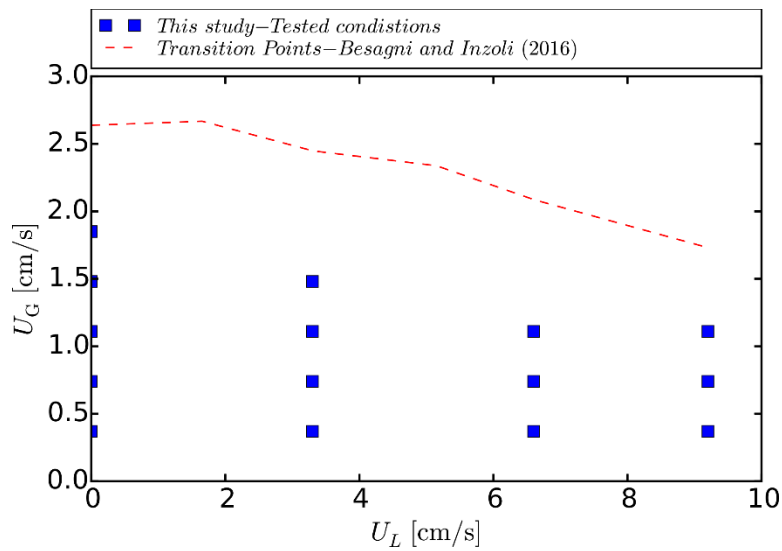
170 This method of moving the camera in radial direction at the two heights is executed for the
 171 15 flow-configuration listed in Table 1 so that in total 330 single experiments were
 172 conducted. The tested conditions are plotted against the determined regime transition
 173 points in Figure 4: all experiments are situated below the transition point in the pseudo-
 174 homogenous regime. In fact, the flow configurations were determined by the optical
 175 accessibility of the flow field from the outside. As will be discussed in the following sections,
 176 above 6 or 8 % integral gas holdup, depending on the bubble size, meaningful
 177 measurements with the present technique were not possible in this large-diameter column.

178 Table 1 Operating conditions evaluated in the present study (marked as ✓); in brackets is
 179 the integral gas holdup at this operation point given (Besagni and Inzoli, 2016a).
 180 Accordingly with the uncertainty analysis on the gas holdup measurements proposed in

181 (Besagni et al. 2017), the gas holdup are measured with an absolute error estimated below
 182 ± 0.02 %.

Sup. gas velocity [cm/s] → Sup. liquid velocity [cm/s] ↓	0.37	0.74	1.11	1.48	1.85
0.0 (batch mode)	✓ (1.02 %)	✓ (1.64 %)	✓ (3.72 %)	✓ (5.30 %)	✓ (6.60 %)
-3.3 (counter-current mode)	✓ (1.32 %)	✓ (2.91 %)	✓ (4.61 %)	✓ (6.63 %)	
-6.6 (counter-current mode)	✓ (1.70 %)	✓ (3.62 %)	✓ (5.99 %)		
-9.2 (counter-current mode)	✓ (2.44 %)	✓ (5.00 %)	✓ (7.55 %)		

183



184

185 Figure 4 Operating conditions evaluated in the present study (blue) compared with the
 186 regime transition point (red line) determined by Besagni & Inzoli (2016a).

187 With tracer particles glued between glass plates, the 2 mm depth of field of the camera
 188 setup was calibrated as described in our previous work (Ziegenhein et al. 2016a). The
 189 aperture of the lens and the thresholds of the post processing algorithms were adjusted to
 190 a depth of field of around 2 mm. It should be noted that the illumination of the particles in
 191 the flow is not the same as in the calibration so that the 2 mm are only a reference value.
 192 However, the used setup is very large compared to the depth of field so that even ± 1 mm
 193 uncertainty is negligible on the 120 mm long radial coordinate. The flow was seeded with 2
 194 g of 50 μm Polyamide 12 particles from DANTEC DYNAMICS A/S with a density of 1010
 195 kg/m^3 . A set of 10 images with 1000 frames per second was recorded every 2 seconds for
 196 1000 seconds for all 11 measuring planes so that in total 55 000 images in 3 hours
 197 measuring time were recorded per operation point. This procedure was equal for all 15
 198 operating conditions at both measuring heights resulting in 1.65 million images.

199 In the following sections, mainly two averages will be used. For the transient results, the
 200 average over the measuring plane and over the burst of 10 images (9 sets of images from
 201 which the particles can be tracked) is used, i.e.

$$\langle v \rangle (T_i, R_j) = \frac{1}{9} \int_{T_i + \frac{1}{100}s}^{T_i} \int_{R_j} v(x, t)_{R_j} dA dt, \quad (1)$$

202 With $\langle v \rangle (T_i, R_j)$ the averaged velocity over the measuring plane dA at time T_i and radial
 203 coordinate R_j . The average is calculated over all 10 images recorded in one burst, which is
 204 equal to a time of 1/100 s. This average is available every two seconds over the 1000
 205 seconds long measuring period. Every measuring plane P_j has a radial coordinate R_j so that
 206 this average is also a function of the position. For the steady state results, the time-
 207 averaged value over the entire measuring time, $\bar{v}(R_j)$ at the radial coordinate R_j is used, i.e.

$$\bar{v}(R_j) = \frac{1}{T} \int_{1000s}^{0s} \omega \langle v \rangle dt \quad (2)$$

208
 209 , where ω represents the hold processor, which is explained in the following sections, and
 210 $\langle v \rangle$ the velocity calculated from Eq. (1). This average is only a function of the radial
 211 coordinate and can be used for comparison with simulations. The averaging indicators $\langle \rangle$
 212 and $\bar{}$ will be omitted where it is clear which average is meant. When not otherwise stated,
 213 the normal Reynolds stresses are calculated by

$$\overline{v'v'}(R_j) = \frac{1}{T} \int_{1000s}^{0s} \left(\bar{v}(R_j) - v(x, t)_{R_j} \right)^2 dt \quad (3)$$

214
 215 , where $v(x, t)_{R_j}$ are the instantaneous velocities measured on plane R_j .

216 2.3 Optical distortion

217 Due to the different refraction indices from air and water, an optical distortion is present.
 218 As mentioned above, the distortion due to the round geometry is handled with a square box
 219 around the bubble column. This is a common technique and therefore the error due to this
 220 is neglected at this point. Moreover, the camera was carefully aligned to the box around the
 221 column so that it is assumed that the view is perpendicular. Nevertheless, the light beams
 222 are not hitting the lens perpendicular, which causes a negligible bending of the depth of
 223 field. This error is discussed in Appendix C.

224 3 Particle Tracking Velocimetry (*PTV*)

225 The used *PTV* method can be separated in two steps, the particle identification and particle
226 tracking. Both methods are shortly discussed in the following subsections, and a detailed
227 description can be found in (Hessenkemper & Ziegenhein 2018). A sampling bias is present
228 in multiphase flows due to the coupling of the dispersed phase with the continuous phase.
229 The sampling bias will be treated with a hold processor, which is shortly discussed in an
230 extra subsection. Detailed information about the sampling bias in dispersed multiphase
231 flows can be found in (Ziegenhein & Lucas 2016b). Finally, we verify the method and the
232 sampling bias treatment by considering the integral values and comparing the *PSTV*
233 method to *PIV* methods in a simplified measurement setup.

234 3.1 Particle Identification

235 Due to the changing background in multiphase flows (Figure 5 (a)) particle identification is
236 not trivial. From our experience, methods based on the gradients calculated from the grey
237 values are applicable. The background has usually small gradients so that a simple
238 threshold on the Euclidian norm of the gradient vector field is working well. However, due
239 to an inhomogeneous illumination of particles the contours are often not closed. To close
240 reliably the contours, a shape recognition algorithm is needed.

241 Shape recognition algorithms are widely used, in particular if simple shapes like circles
242 need to be identified. A relatively robust class of algorithms is based on the Hough
243 transform with which the gradients of a picture (Figure 5 (b)) can be transformed in a
244 parameter space. In contrast to the classic method, the method we use in the present work
245 is a Hough transform based on the pixels that are not on the particle edges. For speed-up,
246 we identify potential particles beforehand. The method is designed for a large amount of
247 small circles rather than identifying a small amount of large circles.

248 However, a main problem of identifying small circles is the representation of such on the
249 grid of the optical sensor. This representation leads to complex shapes, which are irregular
250 and asymmetric. This problem can be handled by evaluating the shape on sub pixel
251 position. Nine points per pixel was a good compromise between accuracy and computation
252 time for the present purpose (Hessenkemper & Ziegenhein 2018).

253 Looking at the discrete representation of circles on a grid, a circle with a specific radius can
254 only have edge pixels in a certain distance around his center. Therefore, when the center
255 (sub-) pixel position is found and the correct radius is known, a specific number of edge
256 particles should be found on this radius. Using this knowledge, the distance to the edge
257 pixels for each sub-pixel position in a radius of three pixels is calculated and distributed in
258 a discrete classification of particle sizes (Table 2). The particle size classification is
259 obtained from the analytical solution of circles on a mesh. The particle size with the largest
260 amount of edge pixels is registered to the sub-pixel position. If two particle sizes have the
261 same amount of edge particles, the larger particle size will be taken. The local maxima of

262 the resulting parameter space are the particle center positions with the assigned particle
 263 size. To avoid spurious particle identification, the introduction of a minimum edge pixel
 264 count for each particle size is necessary. If the count is below this value, the edge particle
 265 count is set to zero.

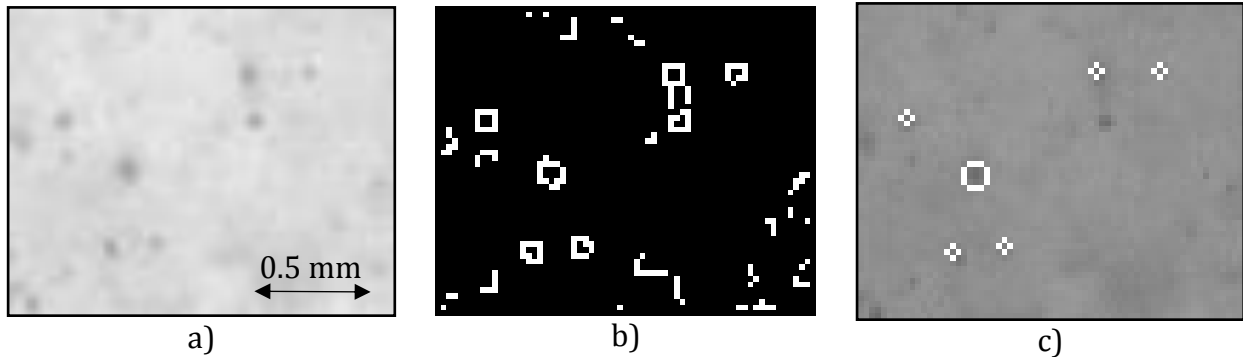
Circle radius [Px]	Set of possible distances [Px ²]	Minimal edge pixels
1.0	$1 \leq D^2 \leq 2.25$	6
1.25	$1 \leq D^2 \leq 3.25$	7
1.5	$1.25 \leq D^2 \leq 4.5$	8
1.75	$2 \leq D^2 \leq 5$	9
2.0	$2 \leq D^2 \leq 6.25$	10
2.25	$5 \leq D^2 \leq 8.5$	12
2.5	$5 \leq D^2 \leq 10.25$	14
2.75	$8 \leq D^2 \leq 12.25$	16
3	$8 \leq D^2 \leq 13$	18

266 Table 2 Classification of the circle size depending on the distance, D, to the edge pixels.

267 An example of the particle identification is shown in Figure 5 (c). Figure 5 shows a bubble-
 268 free, small magnification of the original recorded image (cf. for example Figure 6). The
 269 large particle identified in Figure 5 (c) is an agglomeration of tracer particles or a
 270 microbubble naturally occurring in the flow. Particles or particle agglomerations over 75
 271 μm are not used for tracking, which includes the large particle identified in Figure 5 (c). To
 272 increase the sub-pixel accuracy, the grey values inside the found circles are fitted to a two-
 273 dimensional Gaussian function

$$f(x, y) = A \exp \left[-\frac{(x - x_0)^2}{2\omega_x} - \frac{(y - y_0)^2}{2\omega_y} \right] + \epsilon_{xy} \quad (4)$$

274



275 Figure 5 Magnification of a picture to illustrate the particle identification process. a) Image
 276 for particle identification, b) the gradient field calculated with the Sobel operator with a
 277 threshold and c) the identified particles colored white based on the above-discussed
 278 algorithm (Hessenkemper & Ziegenhein 2018).

279 3.2 Particle Tracking

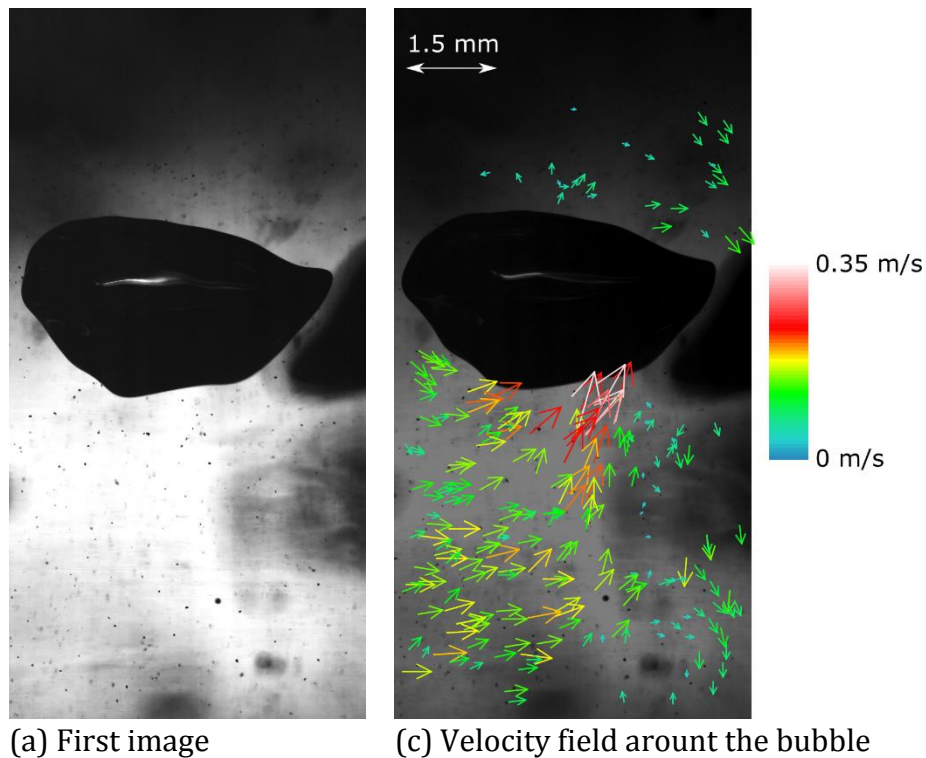
280 For tracking the identified particles, we used a brute force algorithm with a correction step.
281 The basic idea of the algorithm is to find patterns of tracer particles in the subsequent
282 image, which is a combination of classic PTV and PIV algorithm. The method is in detail
283 explained by Hessenkemper & Ziegenhein (2018). A correction step is needed in the
284 present setup since bubbly flows have usually a strong velocity component perpendicular
285 to the measuring plane. Therefore, many tracer particles travel outside the observation
286 area during the measurement. The resulting change of the tracer patterns is causing
287 spurious vectors, which need to be corrected based on the neighboring particle tracks.

288 The identification of outliers is not trivial; a usual approach that uses the standard
289 deviation of the entire set of vectors is not useful since they overweight the outliers.
290 Therefore, a representative set of vectors with which the standard deviation can be
291 calculated is searched. The representative set is determined around the highest
292 concentration of velocities transferred to a discretized velocity map. By using a velocity
293 map, the direction of the velocity is included. The discretization of the velocity map is
294 circular and overlapping to avoid the drawbacks of a rectangular discretization. Identified
295 spurious vectors were re-iterated with the particle-tracking algorithm under the side
296 condition of the averaged velocities found in the cell with the highest velocity count. This
297 procedure was only applied when the velocity count per set of images was higher than ten
298 velocities. The allowable maximum velocity was set to 0.85 m/s, the size of the
299 discretization cells on the velocity map was 0.23 m/s, and 3.5 times of the vector standard
300 deviation in the cell with the maximum velocity count was allowed. The maximum velocity
301 allowed was determined from test measurements where spurious vectors were sorted out
302 by hand and all of the measured velocities were below 0.65 m/s; we added 0.2 m/s to this
303 value in order to capture rare events of high velocities. The size of the cells on the velocity
304 map is chosen arbitrary to the rise velocity of the bubbles in still water. Based on a normal
305 distribution, a standard deviation of 3.5 was chosen so that 99.9% of the velocities are
306 included. With a spatial resolution of around $1.5 \cdot 10^{-7}$ m, we reached a nominal resolution
307 of around 0.0115 m/s per pixel when recording with 1000fps.

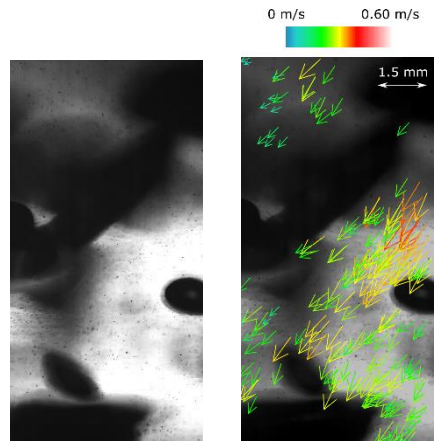
308 The result of the tracking algorithm at a very low gas fraction is shown in Figure 6. The
309 challenges of tracking the velocities for the present case can be seen nicely from this
310 example. From the perspective of particle identification, the image has a very
311 inhomogeneous illumination; while particles in the overexposed areas can be identified
312 easily with the gradient method, the particle edges are hardly distinguishable from the
313 darker background in the under exposed areas. Therefore, the noise is very high in these
314 areas, which would lead to many false particle identifications. However, the particle
315 identification based on the Hough transform gave robust results in these areas compared to
316 other techniques like the Canny algorithm (Canny 1986). From the perspective of particle
317 tracking, the flow field around a bubble is very complex so that high out of plane velocities,
318 a high range of velocities, high shear fields, and small-scale vorticities occur. As explained
319 above, the high out of plane velocity is tried to address by tracking patterns of particles and

320 using a re-iteration correction step. The wide range of flow phenomena at a low resolution
321 is handled by the tracking algorithm well.

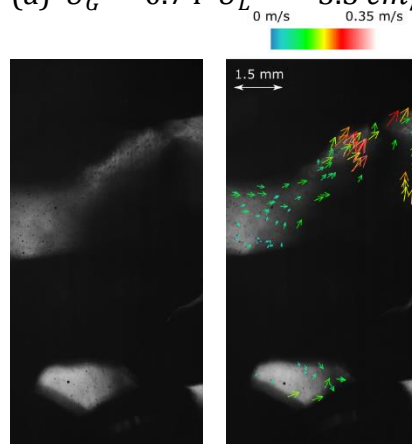
322 While at low gas fractions many particles are visible, the situation is changed at higher gas
323 fractions (Figure 7). At around 7-percentage gas fraction in the 0.24 m thick reactor only
324 small areas in which particles can be tracked are occasionally available. Due to the slip
325 velocity of the bubbles, these areas are closing from one picture to another so that particles
326 are additionally lost. This is causing more and more spurious vectors, which have to be
327 identified, re-iterated and sorted out if necessary. Additionally, this might cause a sampling
328 bias as explained in the following section.



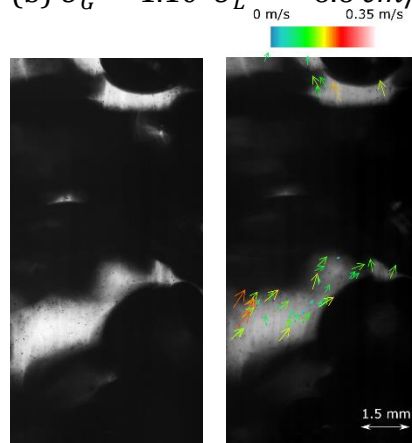
329 Figure 6 Velocity field obtained for a superficial gas velocity of 0.37 cm/s and a superficial
330 liquid velocity of 0 cm/s (batch mode).
331



(a) $U_G = 0.74$ $U_L = -3.3$ cm/s



(b) $U_G = 1.10$ $U_L = -6.6$ cm/s



(c) $U_G = 1.85$ $U_L = -0.0$ cm/s

332 Figure 7 Examples of the measured liquid velocity for different superficial gas and liquid
 333 velocities.

335 3.3 Sampling bias

336 Sampling bias exist in multiple ways in multiphase flows. As discussed in our previous
 337 work (Ziegenhein & Lucas 2016b), a significant bias is present due to the correlation
 338 between the gas volume fraction and the liquid velocities. This correlation is problematic
 339 since high gas volume fractions, which are usually connected to high liquid velocity fields,
 340 block the optical measurements so that less information are measurable in this situation.
 341 This leads to a correlation between the count of measured particle tracks and the velocity,
 342 which leads to a sampling bias. In Figure 8 this correlation is shown for the center of the
 343 column. In Figure 8 are shown the average velocities $\langle v \rangle$ (cf. Section 2.2) and the track
 344 count of this averaging procedure at the different measuring times in the center of the
 345 column. Certainly, more tracks are recorded when the velocity is low and vice versa, which
 346 causes a negative correlation coefficient of -0.288 . A hold processor as developed in our
 347 previous work (Ziegenhein & Lucas 2016b) can now be used to correct this bias. Since we
 348 covered a relatively large measuring area, in almost all recordings some tracked velocities
 349 are present. Therefore, we do not need to wait in time so that we can simplify the hold
 350 processor by just averaging the velocity over the measuring area per time step (i.e. the 10
 351 recorded frames per time step). In order to get the correct, unfiltered Reynolds stresses,
 352 the turbulence parameters take this averaging into account (Ziegenhein & Lucas 2016b). In
 353 Figure 9, the time-averaged values \bar{v} are compared with and without the hold processor.
 354 Every measuring plane gives one value on the radial coordinate. When we look at the
 355 velocity profile over the radius (Figure 9), the effect is larger in the center due to the larger
 356 distance to the camera and therefore a higher gas fraction that can block the camera view.

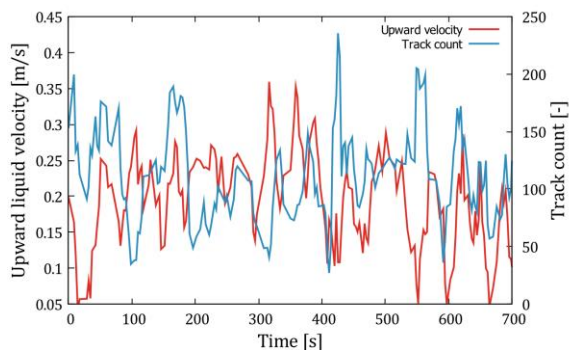


Figure 8 Correlation between liquid velocity and track count for $U_G = 1.48$ cm/s, $U_L = 0$ cm/s in the center of the column.

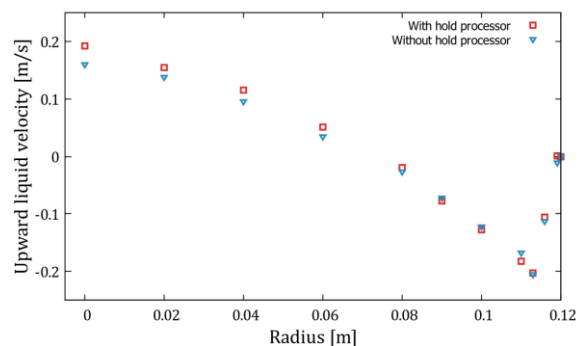


Figure 9 Results with and without hold processor for $U_G = 1.48$ cm/s, $U_L = 0$ cm/s

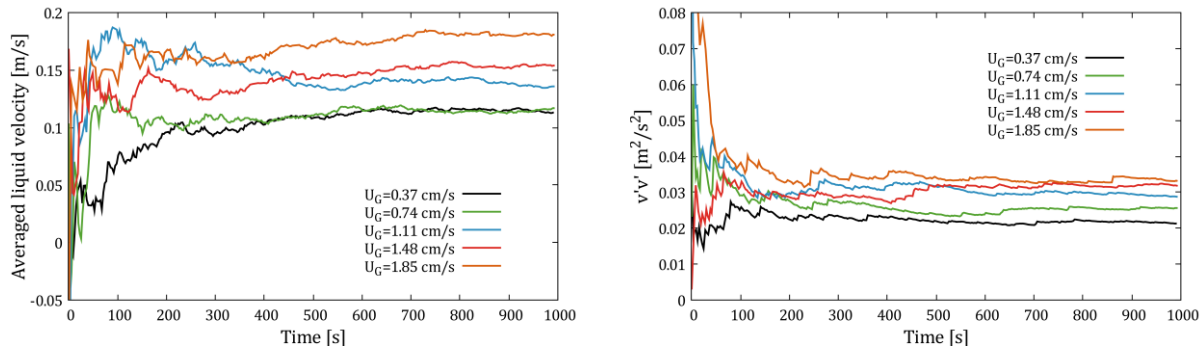
357 Another sampling bias might be obtained because the bubbles are faster moving than the
 358 liquid as explained in the previous section. In principle, we try to catch tracer particles in
 359 spaces between the moving bubbles. If a particle in the first picture is identified right above
 360 a bubble and if the tracer is too slow, it will be blocked in the next picture by the ascending

361 bubble and the track is lost. However, a faster tracer would be not blocked and therefore
 362 tracked. The same mechanism is present if a fast tracer is situated right below a bubble that
 363 is slower ascending and, therefore, not in the measuring plane. However, the effect is
 364 asymmetric due to the upward direction of the rising bubbles so that slower tracers will be
 365 generally more often lost than fast tracers will. The quantification and evaluation of the
 366 effect is difficult so that it will be not treated at this point.

367 3.4 Verification and validation

368 3.4.1 Measuring time

369 Despite the bubble column is operating in the homogeneous regime in which the integral
 370 gas holdup is increasing linear with the superficial gas velocity, a bubble plume with very
 371 long time scales can be observed (Figure 10). After every change of the superficial liquid
 372 and/or gas superficial velocity, we waited 30 minutes before the measuring campaign
 373 began. In Figure 10, the accumulation of the time averaged liquid velocity, i.e. $v(T) =$
 374 $\int_T \langle v(t) \rangle dt$, in the center plane for batch mode is shown. Even after 1000 seconds, the
 375 averaged velocities show some changes over time. Nevertheless, the changes are rather
 376 small so that a 1000-second measuring time was a good compromise between accuracy
 377 and effort; additionally, a 1000-second measuring time has been also used for the optical
 378 probe measurements (Besagni & Inzoli 2016a). Since the normal Reynolds stresses are the
 379 variance of the single velocity components, they converge faster than the averages. The
 380 statistical uncertainty given by $\frac{\sigma}{\sqrt{N}}$ is for the averaged velocity below 0.001 m/s and for $v'v'$
 381 below $0.0003 \text{ m}^2/\text{s}^2$ for all operation conditions.



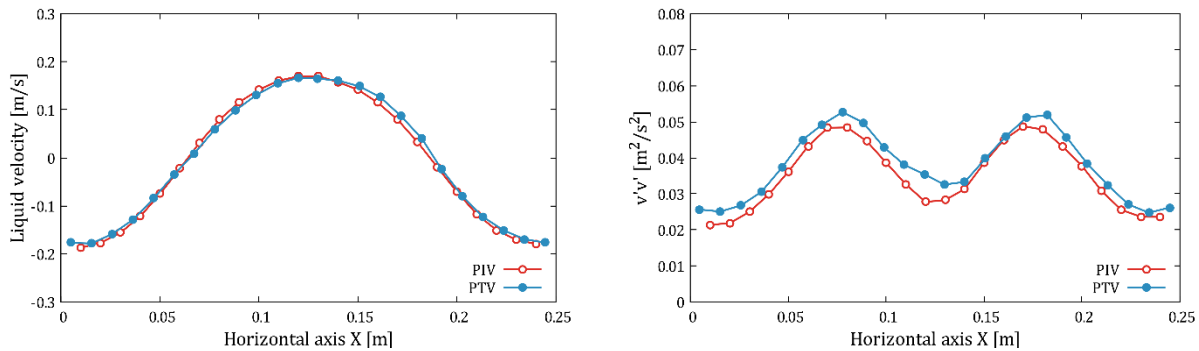
382

383 Figure 10 Accumulation of the averaged liquid velocity and $v'v'$ over time for different
 384 superficial gas velocities in batch mode.

385 3.4.2 Comparison with PIV

386 In our previous work (Hessenkemper & Ziegenhein 2018) we compared the present PSTV
 387 algorithm with PIV measurements in a smaller test bubble column. In this study, the tracer-
 388 particle density was chosen in a way that both methods worked well and the spatial
 389 resolution was adapted to the specific requirements of the specific method. Compared to

390 the present study, the seeding was distinctly higher so that the comparison of PIV and PSTV
 391 in the following shows only that the used PSTV algorithms are valid and applicable to
 392 bubbly flows. The results for a superficial gas velocity of 1 cm/s with comparable bubble
 393 sizes to the present case are shown in Figure 11. The obtained liquid velocity shown in
 394 Figure 11 a) is almost equal for both methods. For the normal component of the Reynolds
 395 stress tensor in upward direction, $v'v'$ shown in Figure 11 b), PSTV delivers slightly higher
 396 values. Since PIV is using interrogation areas that function like a box filter, $v'v'$ obtained
 397 from PSTV measurements are higher in general, which might be the reason for that
 398 deviation.



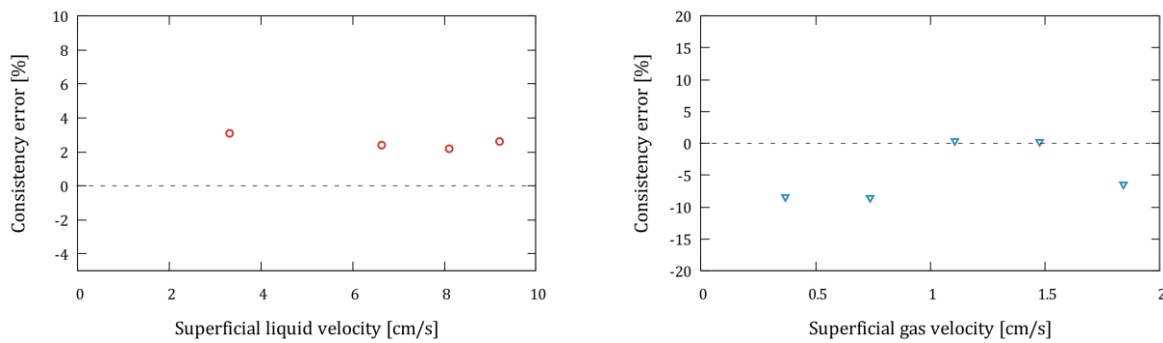
399 Figure 11 Comparison of the present PTV algorithm with PIV measurements from
 400 Hessenkemper & Ziegenhein (2018).

401 3.4.3 Consistency

402 The evaluation of the present methods can be done by calculating the integral properties of
 403 the flow with the local measurements. By integrating the local results, small systematic
 404 errors are summed up and can be therefore easily accessed by evaluating the consistency
 405 between the theoretical and determined properties. The strategy is as follows, with the
 406 liquid velocity field and the void fraction profiles, which are only available for the batch
 407 mode, from the previous measurements in the column, the superficial liquid velocity in the
 408 bubble column can be calculated. The calculated superficial velocity should be zero in batch
 409 mode.

410 As a basic test, we evaluate the superficial liquid velocity without gas 0.7 m above the
 411 sparger. At 0.7 m above the sparger, we assume that inlet effects from the counter current
 412 flow, which is distributed at the top of the column through a basin, are negligible. Under
 413 this condition, we see an overprediction of around 3% (Figure 12 left), which is in the
 414 range of the uncertainty of the mechanical rotameter. It should be emphasized that we only
 415 measure half of the column and cannot consider asymmetric behaviors. Further, it should
 416 be noted, that the consistency error is higher on the upper measuring level at 1.9 m above
 417 the sparger. Therefore, we conclude that asymmetric inlet effects are present at this level
 418 despite the basin of $0.0735 m^3$ on top of the column (Figure 1), particularly at high volume
 419 flow rates. Therefore, we focus in the following on the lower measuring position and the
 420 results of the upper position are given in the Appendix.

421 Another picture is obtained in batch mode at the same measuring position, 0.7 m above the
 422 sparger. Multiplying the measured liquid velocity and the measured liquid volume fraction
 423 (Besagni & Inzoli 2016a), the integration of this product is an estimation for the superficial
 424 liquid velocity. However, since the volume fraction and liquid velocity measurements are
 425 almost one year apart, the correlation between these two values, $\overline{(1-\alpha)'v'}$, is not
 426 included. In Figure 12 right hand side, is the volume flow obtained by integrating the
 427 velocity profile divided by the total recirculation volume flow for batch mode as a
 428 percentage value shown. Considering that the present measurements and the void fraction
 429 measurements are one year apart, that we neglect the correlation $\overline{(1-\alpha)'v'}$, and the
 430 general difficulty to measure liquid velocities in multiphase flows, a deviation of 10%
 431 integral error is very acceptable.



a) Comparing the integration of the liquid velocity profile with the volume flow regulated at the pumping station for Single-phase flow, 0.7 m above sparger

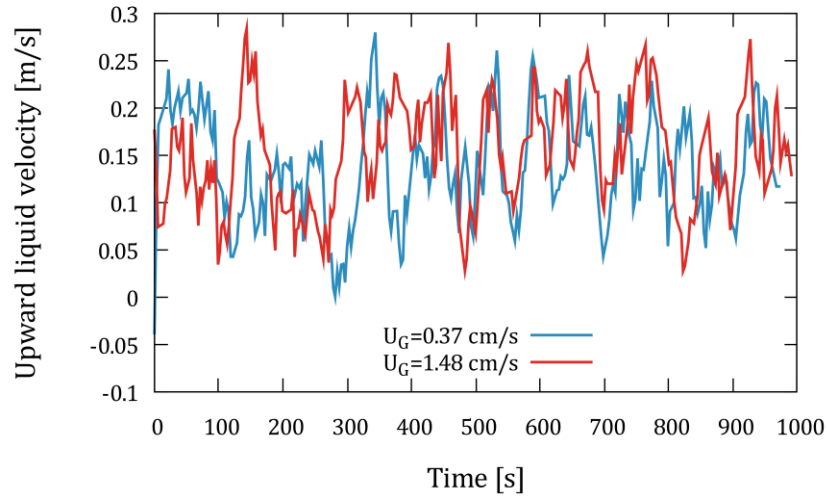
b) Consistency error calculated with the measured gas volume fraction and the liquid velocities in batch mode, 0.7 m above sparger

432 Figure 12 Consistency of the measurements. a) The error of the superficial liquid velocity
 433 without gas for two different fill-heights of the column. b) The lack of the superficial liquid
 434 velocity for different superficial gas velocity without counter current flow and 0.3 m fill
 435 height.

436 4 Experimental results

437 4.1 Long-time, transient behavior

438 Despite in the pseudo-homogeneous flow regime the integral gas holdup is changing linear
 439 with increasing superficial gas velocity (see Figure 28a, in Appendix A), a distinct transient
 440 behavior of a center-plume at both measurement levels can be observed. The upward
 441 liquid velocities, $\langle v \rangle$, in the center of the column for two different gas superficial
 442 velocities ($U_G = 0.32$ cm/s and 1.48 cm/s) in the batch mode are shown in Figure 13. The
 443 transients are moving averages over 6 seconds, which is equal to a low pass filter with a
 444 rectangular function with a size of 6 seconds, to emphasize the very long time scales, which
 445 are characteristic for bubble plumes. In fact, from a Fourier-Transform dominant
 446 frequencies can be obtained (Figure 14).

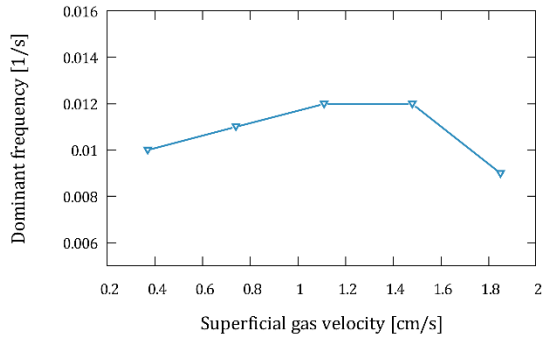


447

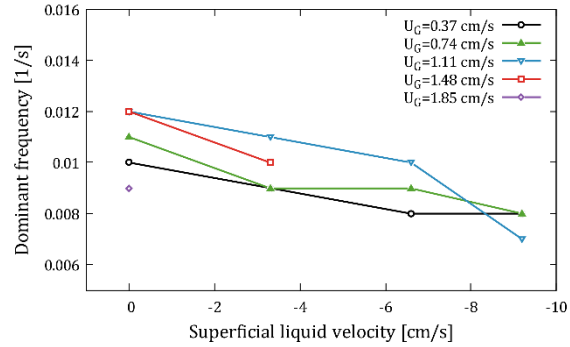
448 Figure 13 Large-scale transient behavior for $U_G = 0.37 \text{ cm/s}$ and $U_G = 1.48 \text{ cm/s}$ for
 449 batch mode, $U_L = 0 \text{ cm/s}$, in the center of the column at the lower measuring level. The
 450 results are moving averaged over 6 seconds. Local, instantaneous velocities can be
 451 therefore distinctly higher.

452 The nominal frequency resolution of the Discrete Fourier Transformation is $1/1000 \text{ 1/s}$,
 453 which is poor since the dominant frequencies are in the range of $1/100 \text{ 1/s}$ (Figure 14 left).
 454 Nevertheless, a trend can be observed that the plume frequency is increasing with
 455 increasing superficial gas velocity, as often reported for tabletop bubble columns. After the
 456 bubble plume frequency is increased, the frequency is decreasing for the highest superficial
 457 gas velocity, which comes close to the flow regime transition (Section 2.2). Such a decrease
 458 needs to be further investigated due to the poor frequency resolution. Nevertheless, the
 459 decrease in frequency is in line with the observations of the authors that at this superficial
 460 gas velocities a very large amount of small bubbles exist, compared to a pure bubble plume
 461 with large bubbles at lower superficial gas velocities.

462 Another observation is that with increasing superficial liquid velocity in the counter-
 463 current flow setup (Figure 14 right), the frequencies are decreasing for all gas velocities.
 464 Probably, the rotation of the counter-current liquid flow due to inlet effects hinders the
 465 natural rotation of the bubbly flow, as discussed in the next section, and therefore
 466 influences the plume frequency. However, the counter-current mode destabilizes the
 467 homogeneous flow regime in general. The relationship between plume frequency and the
 468 prevailing flow regime is a matter of future studies.



(a) Batch mode

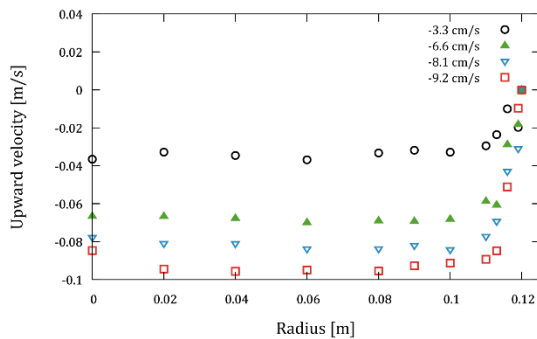


(b) Counter-current mode

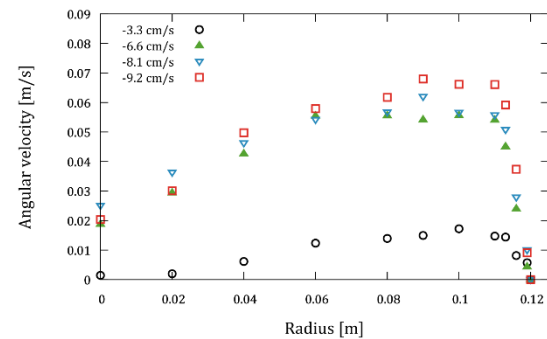
469 Figure 14 Dominant frequencies, obtained by Fourier-Transform of instantaneous
 470 velocities, in the batch mode with varying superficial gas velocities (a) and in the counter-
 471 current mode with varying superficial liquid velocities for different superficial gas
 472 velocities, U_G , (b) evaluated from the velocity transients determined in the center of the
 473 column.

474 4.2 Time averaged liquid velocity profiles

475 The averaged liquid velocity profile, \bar{v} (cf. Eq. (2)), for the single-phase flow without gas is
 476 flat in the center with a steep slope towards the wall (Figure 15a). The single-phase flow
 477 Reynolds number calculated with the pipe diameter as characteristic length scale is ranging
 478 from around 9,000 to 20,000. As expected, the profiles are just shifted to higher absolute
 479 velocities with increasing flow rate. Due to the radial inflow in the basin on top of the
 480 column, the water is rotating in it. This rotation can be clearly seen in the angular velocity
 481 (Figure 15b). From visual observation, this circular current is preserved towards the
 482 bottom of the column. In the angular velocity, an asymmetry can be seen since the sign
 483 change is not in the center of the column for superficial liquid velocities above -3.3 cm/s,
 484 which might explain the inconsistent behavior shown in Figure 12a for a fill height of 0.3 m.



(a) Single-phase flow

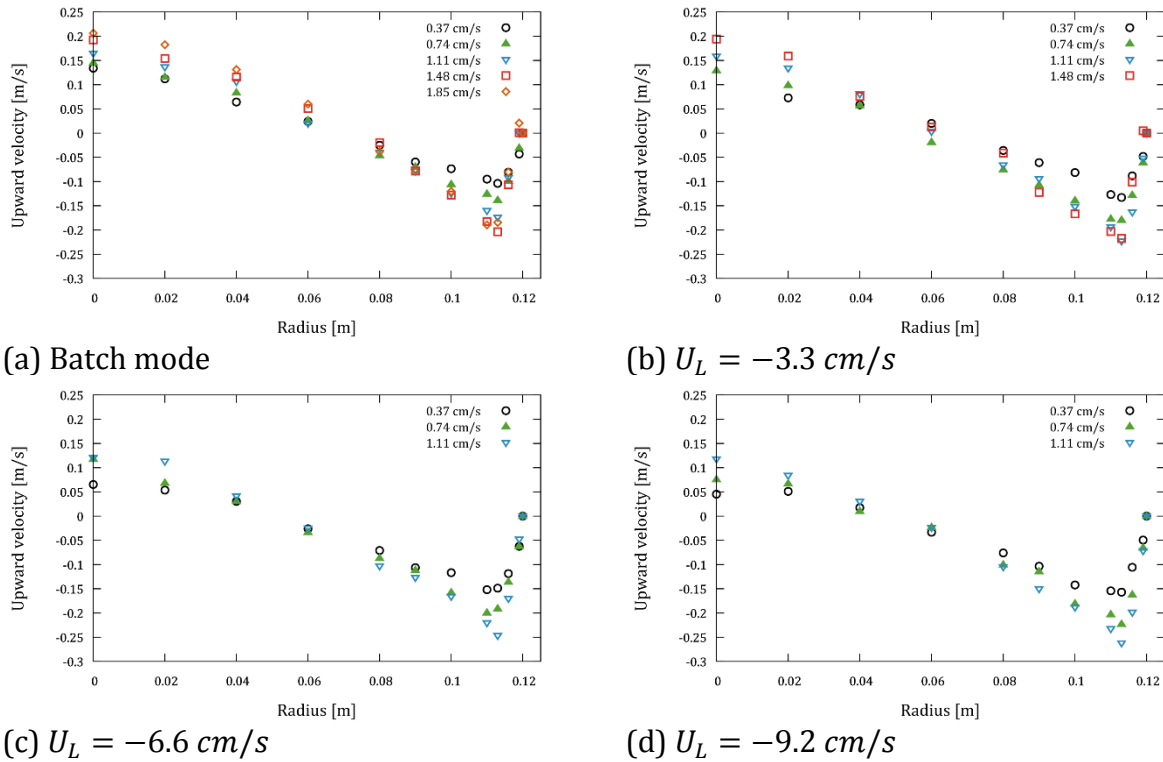


(b) Single-phase flow

485 Figure 15 Averaged velocities without gas ($U_G = 0 \text{ cm/s}$) at different superficial liquid
 486 velocities. a) The upward velocity and b) the angular velocity against the column radius.

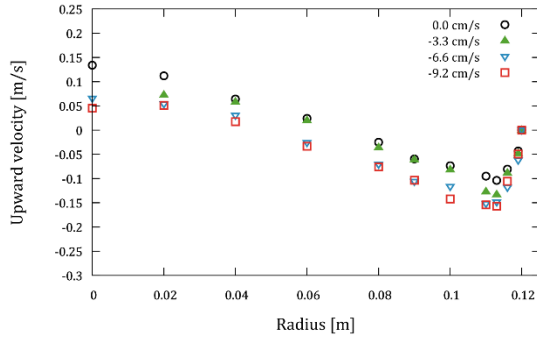
487 The averaged upward liquid velocities for all operations points are compared in Figure 16.
 488 With increasing superficial gas velocity, the gradients in the liquid profiles are getting

489 steeper, which can be nicely seen for the batch mode. For all operation points, the point of
 490 minimum velocity is situated around 0.075 mm away from the wall. The shape of the liquid
 491 velocity profile is as the one reported in the pioneering study of Ueyama & Miyauchi
 492 (1979). The liquid phase flows upward in the center of the column, it becomes zero at an
 493 intermediate radial position (close to $r/\sqrt{2}$) and, finally, it flows downward near the wall.
 494 The reader may refer to Appendix B for the data obtained at $h = 1.9$ m above the gas
 495 sparger, where similar consideration can be applied.

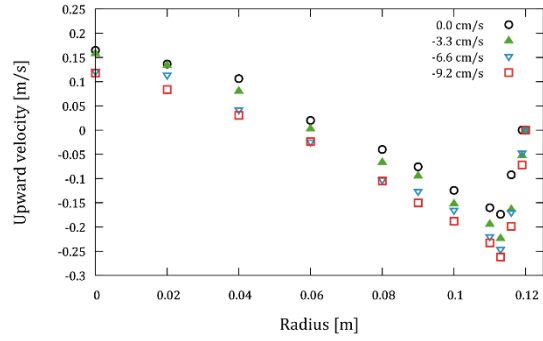


496 Figure 16 Averaged upward liquid velocities for different superficial gas velocities at
 497 different superficial liquid velocities, U_L , 0.7 m above the gas sparger.

498 The influence of the counter-current flow is emphasized in Figure 17. Overall, the velocity
 499 profiles are just shifted downwards due to the superficial liquid velocity. This observation
 500 is consistent with our previous observations that are summarized in Appendix A (Figure
 501 28, 29 and Figure 30). Further, this is also the assumptions made by Trivedi et al. (2018),
 502 who predict the velocity field in counter-current bubble columns, which is correct for the
 503 present flow configurations.



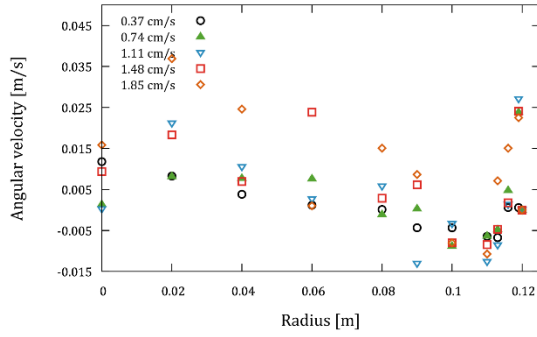
(a) $U_G = 0.37 \text{ cm/s}$



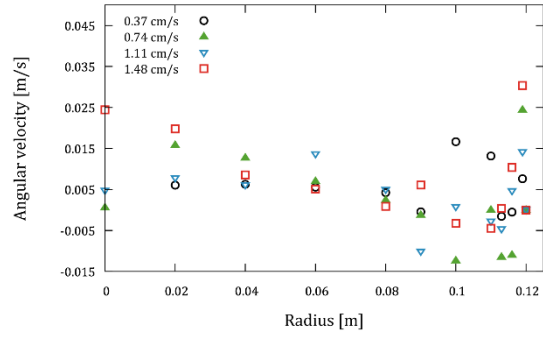
(b) $U_G = 1.11 \text{ cm/s}$

504 Figure 17 Averaged upward liquid velocities for different counter-current flow setups at
 505 different superficial gas velocities 0.7 m above the gas sparger.

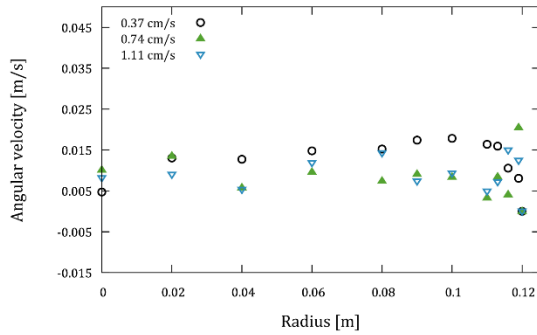
506 The angular velocity, which is for the present measuring setup equal to the measured
 507 horizontal liquid velocity due to the small observation plane (cf. Section 2.2), is changing
 508 distinctly with increasing liquid superficial velocity (Figure 18). The bubbly flow generates
 509 a clear circulating flow, which is changing its direction several times towards the center.
 510 This counter-current angular flow less influences when the liquid velocity is increased
 511 to $U_L = -3.3 \text{ cm/s}$. Due to the radial inflow in the basin on top of the column, the
 512 circulating flow of the liquid inflow (Figure 15) dominates the bubbly flow at $U_L =$
 513 -6.6 cm/s and $U_L = -9.2 \text{ cm/s}$.



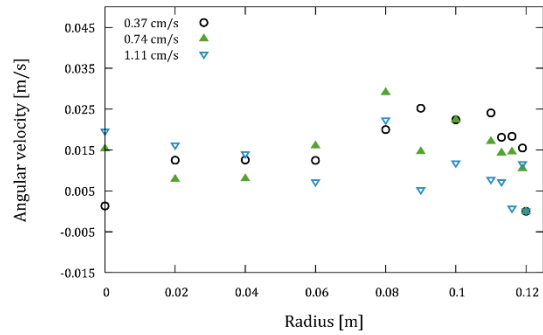
(a) Batch mode



(b) $U_L = -3.3 \text{ cm/s}$



(c) $U_L = -6.6 \text{ cm/s}$

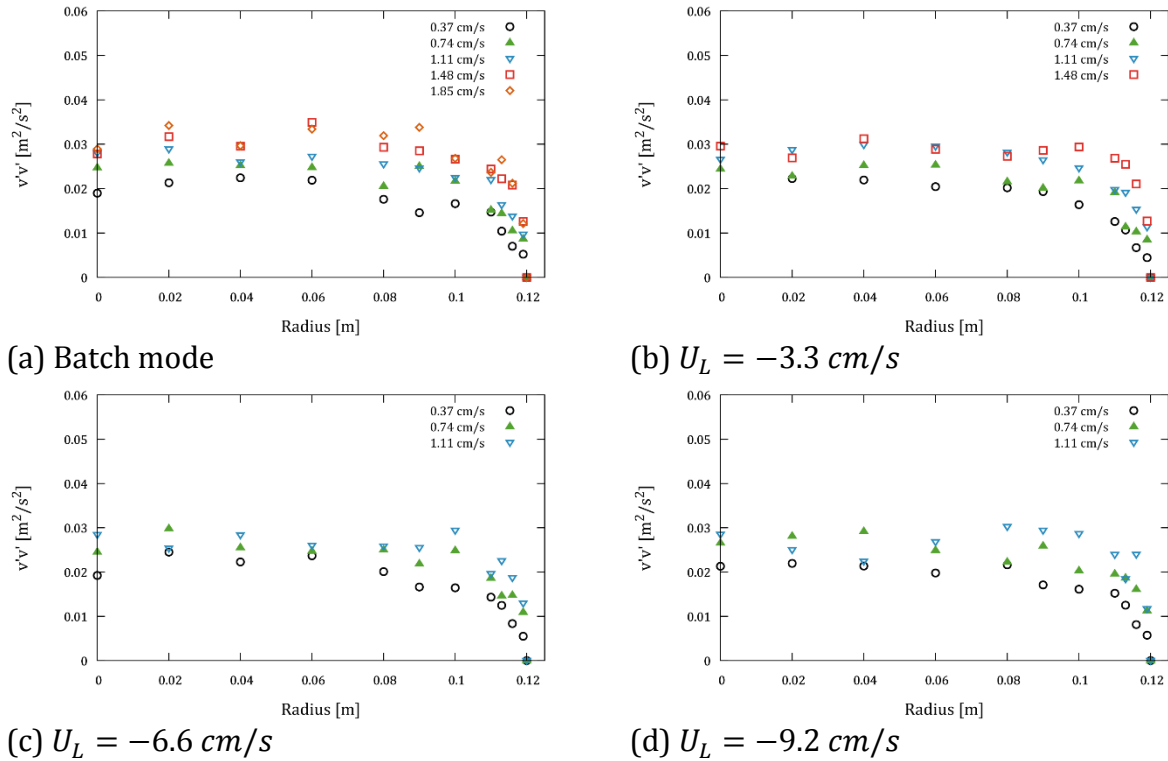


(d) $U_L = -9.2 \text{ cm/s}$

514 Figure 18 Averaged angular liquid velocities for different superficial gas velocities at
515 different counter-current flow setups 0.7 m above the gas sparger.

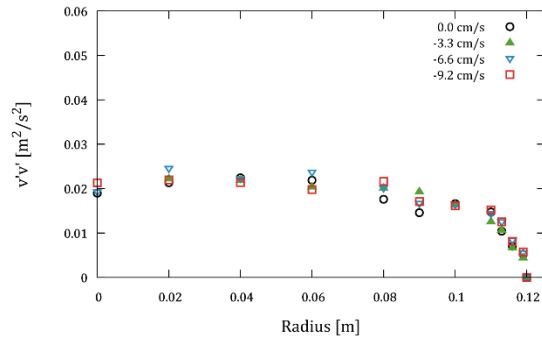
516 **4.3 Normal Reynolds stresses**

517 The normal Reynolds stress tensor component in upward direction, $v'v'$, is almost zero for
518 the single-phase liquid downflow. Increasing the gas flow rate, $v'v'$ is increasing (Figure
519 19) for all counter current flow rates. This increased $v'v'$ rate might have two origins. First,
520 the gas hold-up is increasing, which increases the small-scale turbulence. Second, the
521 plume frequency is increasing with increasing superficial gas flow rate (Figure 14) so that
522 the very large transient scales increase. The almost equal $v'v'$ obtained for $U_G = 1.48 \text{ cm/s}$
523 and $U_G = 1.85 \text{ cm/s}$ in batch mode can be explained by the decreasing plume frequency at
524 $U_G = 1.85 \text{ cm/s}$ (Figure 14), which indicates a damping of the very large transient scales.

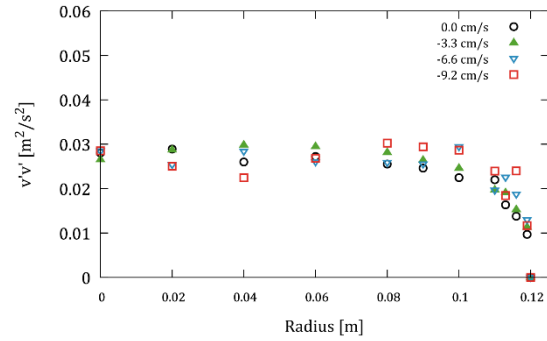


525 Figure 19 Normal Reynolds stresses in upward direction for different superficial gas
 526 velocities at different counter-current flow setups 0.7 m above the gas sparger.

527 Certainly, the counter-current liquid flow is increasing the gas hold-up (see Figure 28a in
 528 Appendix A) so that in principle $v'v'$ should be increasing with increasing superficial liquid
 529 velocity. Surprisingly, $v'v'$ is not or only minor changing for different superficial liquid
 530 velocities (Figure 20). This might be explained by the damping of the plume frequency and
 531 therefore the large scales when the superficial liquid velocity is increased (Figure 14). This
 532 reduction of the large scales might cancel out the effect of higher gas volume fractions in
 533 total. In fact, with the method discussed in the next section to separate the large and small
 534 scale, it will be shown that a filtered $v'v'$ is increasing with increasing superficial liquid
 535 flow rate.



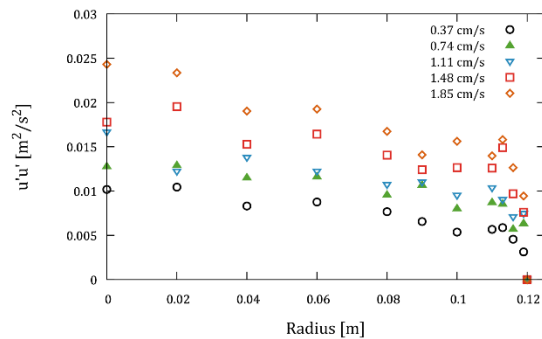
(a) $U_G = 0.37 \text{ cm/s}$



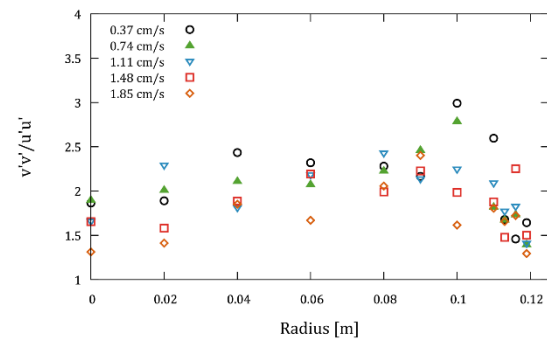
(b) $U_G = 1.11 \text{ cm/s}$

536 Figure 20 Normal Reynolds stresses in upward direction for different counter-current flow
 537 setups for a superficial gas velocity of 0.37 cm/s (a) and 1.11 cm/s (b), 0.7 m above the gas
 538 sparger.

539 The angular component of the Reynolds stress tensor ($u'u'$) (Figure 21) is behaving very
 540 similar to the upward direction. Certainly, the large-scale fluctuations are also present in
 541 angular direction so that $u'u'$ is also influenced by the plume frequency. This behavior of
 542 the system might also significantly influence the ratio of the upward and angular
 543 component (Figure 21). $v'v'$ is dominating around 2 cm away from the wall whereas
 544 towards the center the ratio is decreasing towards 1.5 . Changing the superficial liquid and
 545 gas velocity does not change the ratio significantly.



(a) Batch mode



(b) Batch mode

546 Figure 21 Normal Reynolds stresses in angular direction for the batch mode (a) and the
 547 ratio of normal upward and angular tensor components in batch mode (b), 0.7 m above the
 548 gas sparger for different superficial gas velocities.

549 4.4 Filtered normal Reynolds stresses

550 Filtering the transient velocity results is a method to mask the influence of the large-scale
 551 fluctuations of the meandering bubble plume. The intention of this process is to study the
 552 smaller scales that might be dominated by the bubble-induced turbulence. Due to the filter,
 553 the scales are separated as is usually done in LES. The similarities to LES are obvious, due
 554 to the measurement concept of recording planes in bursts; a filter in space can be used that
 555 is accessible at different time steps. However, the choice of potential filter sizes is limited

556 due to the restrictions of the measurements. Therefore, for all operation points the same
 557 filter will be used and the focus will not be on the absolute value of the filtered turbulent
 558 kinetic energy but on the change with the volume fraction.

559 Looking at the bubble-induced turbulence scale, the important effects are on a length scale
 560 comparable to the bubble size (Ma et al. 2017). In the present setup, the bubbles are
 561 between 3 and 6 mm large (Besagni and Inzoli, 2016a) so that the 6 mm width of the
 562 measurement plane is a good choice for the filter in angular direction. We choose the height
 563 of the filter in stream-wise direction to the complete height of the measuring plane – 25.3
 564 mm – in order to increase the statistics compared to a 6 mm x 6 mm box. However, at lower
 565 void fraction where a very large amount of tracers is trackable, similar results are obtained
 566 with a 25.3 mm x 6mm and a 6 mm x 6mm box.

567 The time scale of the bubble-induced turbulence might be connected to the ratio of slip
 568 velocity and bubble size (Ma et al. 2017). With a slip around 23 cm/s (Tomiyama 2002)
 569 and an averaged bubble size around 4 mm, a characteristic frequency for the bubble-
 570 induced turbulence is found to be around 60 Hz. Lance & Bataille (1991) measured the one
 571 dimensional energy spectra in homogenous bubbly flows with 5 mm bubbles and reported
 572 the significant range between 100 and 1000 Hz. Averaging the information in time over the
 573 set of 10 pictures recorded each with 1000 Hz, a total frequency of 100 Hz is obtained,
 574 which is near the estimated frequency of 60 Hz and in the measured range from Lance &
 575 Bataille. Summarizing, a reasonable box filtering process is obtained by averaging the
 576 obtained velocities over the measuring plane of 6 mm times 25.3 mm and over 0.01
 577 seconds with the focus on the bubble-induced turbulence.

578 Based on the turbulent kinetic energy, it is possible to state that the suggested filter
 579 satisfies the following equality:

$$\langle v'v' \rangle_{Total} = \langle v'v' \rangle_{HighPassFilter} + \langle v'v' \rangle_{LowPassFilter} \quad (5)$$

580 From the explanations above, the low pass filter would be

$$\langle v'v' \rangle_{LowPassFilter} (R_j) = \frac{1}{T} \int_{1000s}^{0s} \left(\bar{v}(R_j) - \omega \langle v \rangle (T_i, R_j) \right)^2 dt, \quad (6)$$

581 with the formulations given in Equation (1) - (3). This low pass filter means that the
 582 turbulent kinetic energy is calculated with the overall averaged velocity, $\bar{v}(R_j)$, and the
 583 averaged velocity over the 10 burst and the measuring plane $\langle v \rangle (T_i, R_j)$, which is
 584 weighted by the hold processor.

585 The high pass filter is than only the turbulent kinetic energy inside the 10 bursts. This can
 586 be obtained by subtracting the low pass filter from the total value, or by calculating the
 587 value from the measured values. In the following, the calculation will be shown, and
 588 Equation (5) will be used to check the results. At first, the filtered turbulent kinetic energy

589 is obtained by calculating the averaged velocity over the set of 10 pictures, $\langle v \rangle$ (cf.
 590 Equation (1)); afterwards, the fluctuations are calculated with this averaged velocity for
 591 every tracked particle:

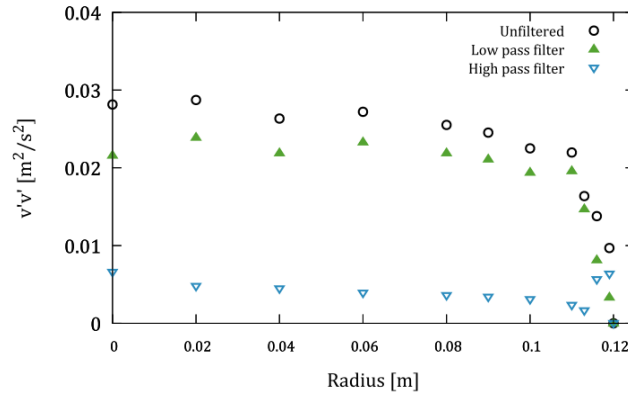
$$\langle v'v' \rangle_{HighPassFilter} (T_i, R_j) = \frac{1}{9} \int_{T_i + \frac{1}{100}s}^{T_i} \int_{R_j} \left(\langle v \rangle - v(x, t)_{R_j} \right)^2 dAdt, \quad (7)$$

592 In the end, the turbulent kinetic energies are averaged over the complete 1000 seconds
 593 measuring time, which includes 500 sets of 10 pictures per measuring point:

$$\bar{v}(R_j) = \frac{1}{T} \int_{1000s}^{0s} \omega \langle v'v' \rangle (T_i, R_j) dt, \quad (8)$$

594 with ω again the weight from the hold processor as discussed in Section 3.3. The sum of
 595 both filter process is equal to the total value of the turbulent kinetic energy, as expected.
 596 Certainly, the made assumptions regarding the filter size in space and time are rough so
 597 that the absolute values that will be obtained with the filtering process should be
 598 interpreted with care. Nevertheless, the change of the obtained values with the volume
 599 fraction is in the focus, which is less sensitive to the filter sizes when they are in the range
 600 of the bubble-induced turbulence.

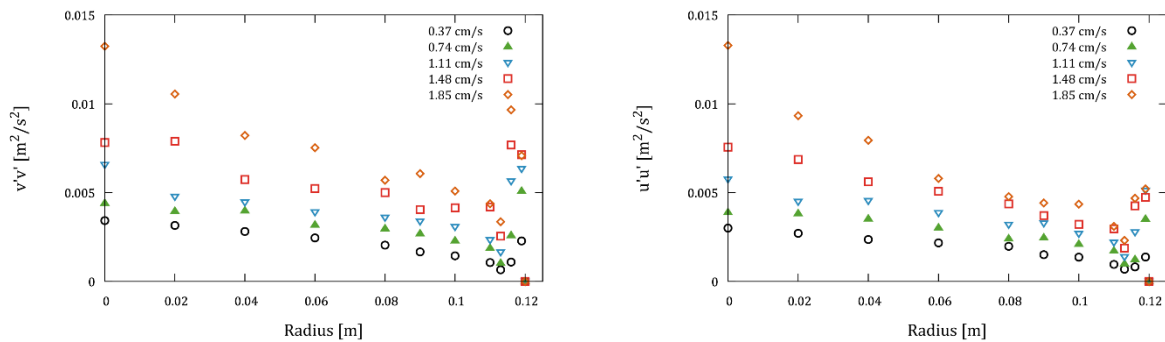
601 The filtered values are compared to the unfiltered in Figure 22. As expected, due to the
 602 non-homogenous distribution of the gas fraction and the resulting bubble plume, the high-
 603 energy scales are the very low ones causing the low pass filter to be distinctly higher. The
 604 high pass and low pass filtered values approach each other towards the walls where the
 605 large scales are damped. When the y-axis is scaled properly for the high pass filtered values
 606 (Figure 23), these values increase towards the center whereas the values for the low pass
 607 filtered values are more or less constant from $r = 0.1$ on. The high pass filtered $v'v'$ values
 608 increase in the same amount as the gas void fraction values towards the center of the
 609 column, which will be discussed in detail below. This is a hint that our filtering actually is in
 610 the turbulent scales that depend directly on the gas void fraction. On the other hand, the
 611 low pass filtered values are dominated by the global flow so that these values are almost
 612 not influenced by the local void fraction distribution.



613

614 Figure 22 Comparison of filtered and unfiltered turbulence data for a superficial gas
 615 velocity of 1.11 cm/s in batch mode.

616 From now on only the high pass filtered values are in the focus. the obtained filtered values
 617 over the radius for all batch mode operation-points are shown in Figure 23. Compared to
 618 the unfiltered values, the filtered values are increasing nicely with the superficial gas
 619 velocity. Near the wall, they have a maximum, which might be explained due to the high
 620 shear rates there. Surprisingly, near the velocity minimum, the filtered values have a
 621 minimum. From this point, the values for all operation points are increasing steadily
 622 towards the center.

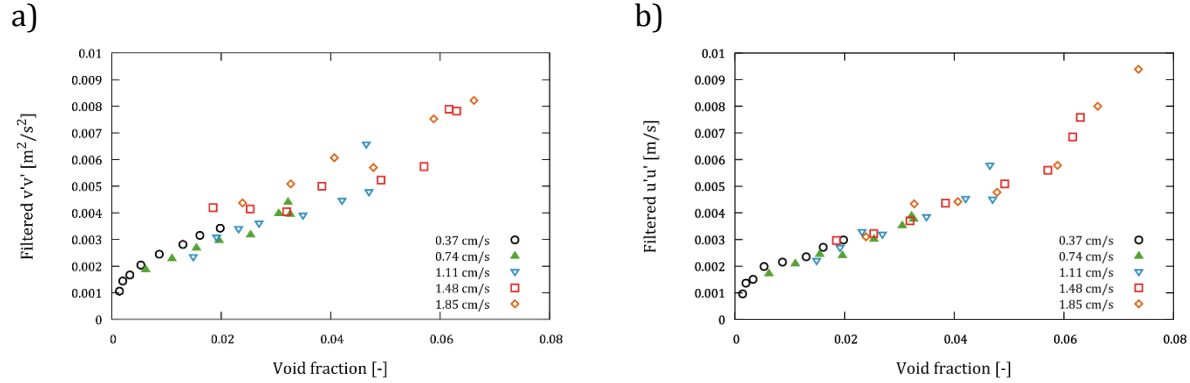


(a) Batch mode

(b) Batch mode

623 Figure 23 Filtered normal Reynolds stresses in upward (a) and angular (b) direction for
 624 batch mode at different superficial gas velocities 0.7 m above the gas sparger.

625 With the volume fraction profiles measured for the batch mode by Besagni & Inzoli
 626 (2016a), every local filtered value from Figure 23 can be assigned to a local volume fraction
 627 (Figure 24). Since the volume fractions were measured at slightly different position, the
 628 void fraction values were interpolated using the void fraction profile by second order to the
 629 locations where the liquid velocities had been measured. Since the wall effects are not in
 630 the focus, only the values from 0 to 0.1 m radius will be considered in the following. The
 631 values obtained for different superficial gas velocities at different position are overlapping
 632 for $v'v'$ and $u'u'$. Moreover, they behave almost linear with a strongly decreasing trend
 633 towards zero volume fraction.

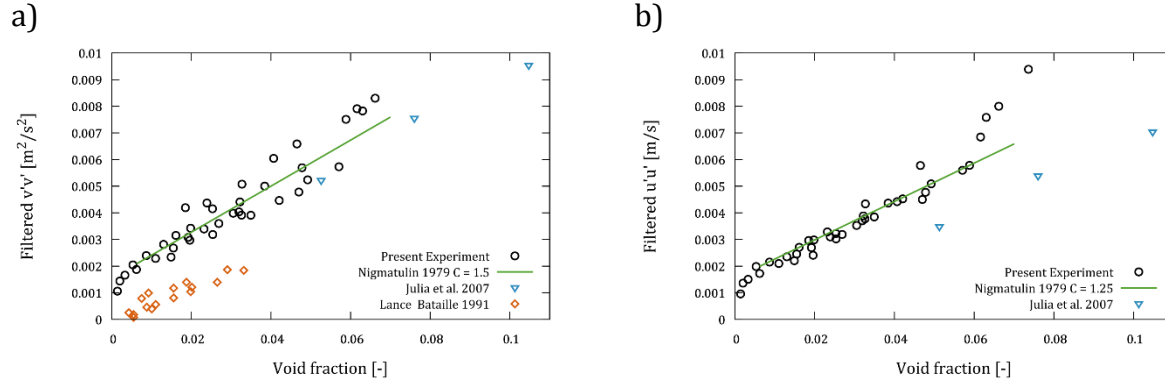


634 Figure 24 Filtered normal Reynolds stresses in upward (a) and angular (b) direction for
 635 batch mode at different superficial gas velocities plotted against the gas volume fraction.

636 A linear trend of the bubble-induced turbulence with increasing volume fraction,
 637 α , for pure homogenous flow without a turbulent background flow was for example
 638 postulated by Nigmatulin (1979) with the formulation

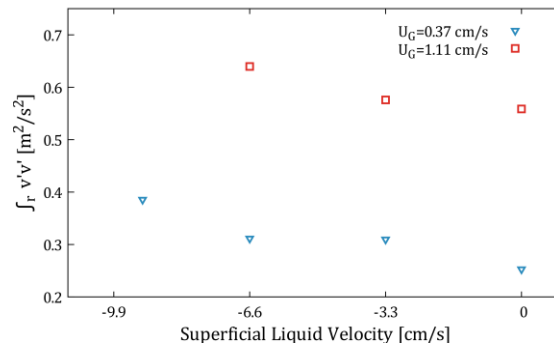
$$k_{L,BIT} = C |\vec{v}_{rel}|^2 \alpha. \quad (9)$$

639 With v_{rel} the slip velocity, which is fixed to 23 cm/s in the following. For the model
 640 constant C different formulation exist; e.g., Lopez de Bertodano et al. (1996) used a
 641 formulation connected to the virtual mass coefficient, C_{VM} , $C = 0.5C_{VM}$ or Julia et al. (2007)
 642 used $C = 1$ to fit their measured $v'v'$ values. For the present results, a model constant of 1.5
 643 for $v'v'$ and 1.25 for $u'u'$ would fit the slope for increasing the volume fraction (Figure 25).
 644 However, the results from Figure 24 indicate a non-linear onset of the turbulence at very
 645 low volume fractions. Therefore, we add a constant factor to Equation (9) to cover the
 646 linear trend from 0.005 gas volume fraction (Figure 25). This constant factor might be
 647 determined by the chosen filter size and is therefore not of significance at this point.
 648 However, the measurements of Julia et al. (2007) are close to the present measurements in
 649 absolute height and slope. The measurements of Lance & Bataille (1991) are a factor of two
 650 lower but with a similar slope. It should be noted that both, the measurements of Julia et al.
 651 and Lance & Bataille, are executed in small table top bubble columns in a pure homogenous
 652 regime without a bubble plume and an almost monodisperse bubble size distribution,
 653 which is substantially different to the present experimental setup.



654 Figure 25 Filtered Reynolds stresses in upward and angular direction compared to other
 655 experiments in batch mode and Eq. (9).

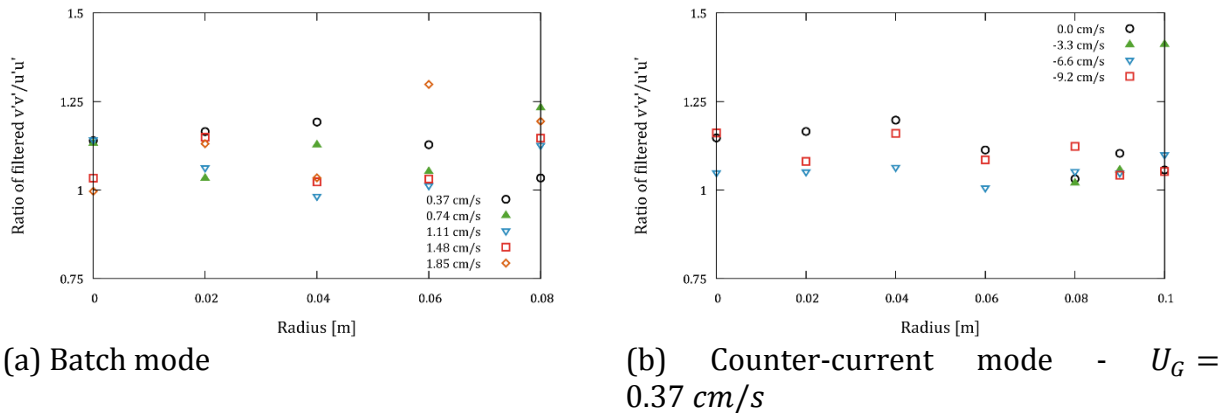
656 The inconsistency described in the previous section of constant $v'v'$ values with increasing
 657 superficial liquid velocity and therefore increasing volume fraction (Figure 20) is
 658 eliminated by using the filtered values. In Figure 26 the integral of the filtered $v'v'$ over the
 659 radius is shown in order to emphasize the total change of $v'v'$ with the increasing liquid
 660 volume flow rate. As expected, the filtered $v'v'$ results are increasing with increasing
 661 superficial liquid velocity so that the assumption that the damping of the large scales with
 662 increasing superficial liquid velocity are counteracting the increasing trend of the small
 663 scales with the volume fraction is reasonable. Unfortunately, for the counter-current flow
 664 setup no volume fraction measurements are available so that these values cannot be added
 665 to Figure 25.



666
 667 Figure 26 Integrated $v'v'$ over the column radius for different counter-current flow setups
 668 for a superficial gas velocity of 0.37 cm/s and 1.11 cm/s, 0.7 m above the gas sparger. The
 669 superficial liquid velocity is increasing towards negative numbers.

670
 671 The ratio of the small scale $v'v'$ and $u'u'$ (Figure 27) are distinctly smaller than the non-
 672 separated ones (Figure 21) and more or less constant over the radius between values of
 673 1.25 and 1.0. In the literature different values for the ratio can be found ranging from 2.0

674 (Julia et al. 2007) to 1.0 (Lance & Bataille 1991). The ratio seems to be not significantly
 675 influenced by the superficial liquid velocity (Figure 27 b).



676 Figure 27 Ratio of $v'v'$ and $u'u'$ for different superficial gas velocities in batch mode (a) and
 677 for different superficial liquid velocities at $U_G = 0.37 \text{ cm/s}$ (b), 0.7 m above the gas
 678 sparger.

679 5 Conclusions, outcomes and outlooks

680 Data sets that include the void fraction, bubble size, and liquid velocity are vital for
 681 validating CFD codes in bubbly flows. In particular, data sets for different facility sizes are
 682 important to validate the capability of present CFD for upscaling. While some data exist for
 683 tabletop bubble columns, complete data sets for larger-scale bubble columns are rare. In
 684 the present study, prior measurements of the void fraction and bubble size (Besagni and
 685 Inzoli, 2016a) were completed with liquid velocity and basic turbulence measurements for
 686 a pilot-scale bubble column in batch and counter-current flow mode.

687 The measurement setup was as simple as possible by using a shadowgraph technique and
 688 tracking added particles with a PTV algorithm (Hessenkemper & Ziegenhein 2018). The
 689 absence of lasers allowed us to measure the velocity in a large-scale lab where the pilot-
 690 scale column was built. Measurements up to an integral gas holdup of around 8 percentage
 691 were possible in the 24 cm diameter bubble column. In total, 15 measuring points, 5 in
 692 batch and 10 in counter current flow mode, at 2 different heights were investigated.

693 Despite the integral gas holdup is increasing linearly, which is usually referred as
 694 homogenous regime, a distinct transient behavior was observed. Relatively long time
 695 frequencies in the range of 1/100 Hz were identified. Similar but much shorter frequencies
 696 are often described for rectangular columns with a center gas sparger. In principle, the
 697 used industrial spider gas sparger is a scale-up of such setups to round pilot-scale columns.
 698 The general trend of an increasing frequency with increasing superficial gas velocity was
 699 also found in the present study. However, the frequency is dropping for the highest volume
 700 fraction, which might be explained by a higher bubble dispersion that hinders the plume.
 701 Increasing the counter current liquid flow, the frequencies are decreasing for all gas

702 volume flows. It is often reported in the literature that bubble plumes show an asymmetric
703 behavior so that they might prefer one side of the bubble column. In the present work, only
704 measurements were conducted along one radial coordinate so that a potential asymmetric
705 behavior is not covered by the data. This should be considered when the data is used for a
706 potential model validation.

707 Increasing the gas flow rate in batch mode leads to an increasing strength of the
708 recirculation, which is expressed by higher shear rates in the vertical liquid velocity.
709 Increasing the counter current flow only shifts the liquid velocity profiles downward
710 without a distinct impact on the time averaged shear rates. From the angular velocity, we
711 found a distinct counter current circulating flow in batch mode, which is dominated,
712 however, by the rotation of the counter-current liquid flow. The rotating counter-current
713 liquid flow is very likely an inlet effect.

714 The normal Reynolds stress components are the summation of the large-scale frequencies
715 induced by the column geometry and the bubble induced turbulence. The normal stresses
716 are increasing with increasing the superficial gas velocity, as expected. However, when the
717 superficial liquid velocity is increased, the values remain almost constant. Since the gas
718 holdup is higher in counter current flow, a higher turbulence level was expected. However,
719 the damping of the large-scale frequencies due to the counter current flow compensated
720 this trend. A filtering technique was therefore introduced in order to separate these two
721 effects on the turbulence level.

722 The filtering method, which is proposed on findings from previous measurements and
723 evaluations of DNS data, allowed us to investigate the trend of a filtered turbulence. The
724 filtering was designed in order to see the bubble-induced turbulence for the different flow
725 setups. Indeed, it was found that the filtered turbulence level is increasing with the counter
726 current flow setup, as expected, due to the higher gas void fraction. The increase is beyond
727 the single flow turbulence level found with zero superficial gas velocity.

728 The previous local gas void fraction measurements allowed us to plot the filtered
729 turbulence against the gas void fraction. The results obtained for different superficial gas
730 velocities fall on a single linear trend line, which was proposed theoretically in the past.
731 This linear trend was previously confirmed for measurements in small tabletop columns in
732 absolute homogenous, specifically monodispersed bubble-size distributions and flat liquid
733 velocity profiles, flow conditions. However, the present results reveal an onset of the
734 turbulence at low void fractions so that the linear trend is not valid at very low bubble
735 concentrations. This onset is in line with previous evaluation of *DNS* data (Ma et al. 2017)
736 and might be due a misaligned balance of turbulence production and dissipation at the
737 bubbles. All in all, the similarity of the results obtained in small-scale, homogenous bubbly
738 flows and the present setup is an argument that bubble induced turbulence models
739 obtained from the simplified homogenous setups are applicable to large scale facilities and
740 can be therefore used for upscaling.

741 **6 Acknowledgement**

742 This work was partially funded by the Deutsche Forschungsgemeinschaft (DFG) under the
743 project number 335448239.

744

746 A. Fluid dynamics in the bubble column

747 Gas holdup (ε_G), local gas volume fraction ($\varepsilon_{G,Local}$), absolute bubble velocity (v_b) and BSDs
748 were measured by Besagni & Inzoli (2016a) beforehand with a bed expansion technique, a
749 double fiber optical probe and image analysis, respectively. Detailed information
750 concerning the used instrumentation, methods, and uncertainties can be found in the
751 descriptions of Besagni & Inzoli (2016a). The results are shortly summarized in the
752 following to help the reader to understand the discussions in the result section.

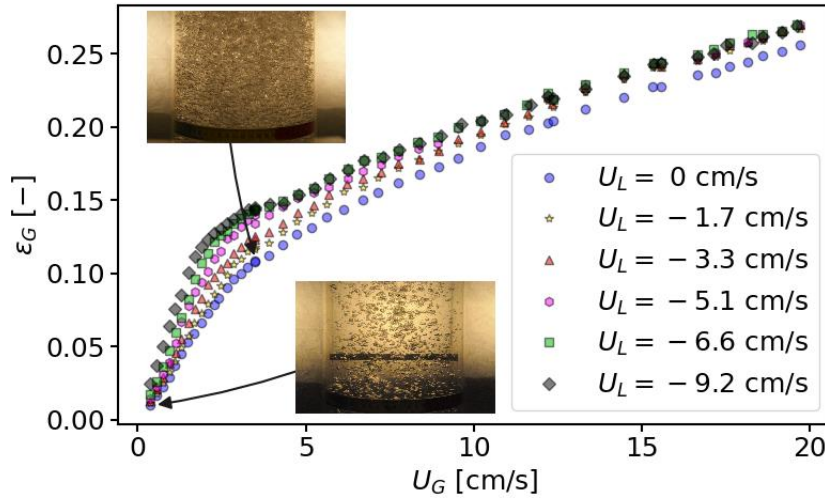
753 Figure 28 displays the gas holdup curves and the flow regime transitions ($\varepsilon_{G,trans}$ and
754 $U_{G,trans}$), between the homogeneous and the transition flow regimes for the batch and
755 counter-current mode. The liquid velocity measurements were conducted up to a void
756 fraction of 7.55 % at $U_L = -9.2$ cm/s. In this region, the gas holdup is monotonically
757 increasing; however, due to the large sparger holes, a polydisperse bubbly flow is present
758 with large bubbles (Figure 29). Moreover, the gas void fractions profiles (Figure 30) show a
759 center peak. Since a homogenous flow regime is usually associated with a monodisperse
760 BSD and a flat void fraction profile, the present regime is called pseudo-homogenous flow
761 regime.

762 The linear behavior of the gas holdup with the superficial gas velocity is changing at the
763 transition point to a pure inhomogeneous regime. In the inhomogeneous regime, larger gas
764 structures can escape the column so that the slope of the holdup is lower compared to the
765 pseudo-homogenous regime. A regime transition theory based on the linear stability
766 analysis of the local force balance is for example given by Lucas et al. (2005). The transition
767 from (pseudo-) homogenous to inhomogeneous is usually fluent so that an intermediate
768 regime, the transition regime, can be identified. Methods to identify the transition point are
769 for example discussed by Besagni et al. (2018).

770 The counter-current flow has the effect that the absolute bubble velocity is reduced (Figure
771 30f) so that the local gas void fraction increases (Figure 30e). Therefore, the slopes of the
772 gas holdup curves in the pseudo-homogenous regime are steeper when the superficial
773 liquid velocity is increased (Figure 28a). This leads to an earlier transition with respect to
774 the superficial gas velocity; but, the transition occurs at higher gas holdups. Since the
775 regime transition is usually connected to coalescence events, this shift of the transition
776 point towards higher gas holdups might be connected to the BSDs produced by the spider-
777 sparger, which are less influenced by the counter-current flow.

778 Following the stability analysis of Lucas et al. (2005) bubbles smaller than 5.8 mm have a
779 positive lift force coefficient (Tomiya et al. 2002) and travel to the column wall and,
780 therefore, stabilize the flow regime. That small bubbles accumulate at the wall was indeed
781 identified in the experiments (Besagni & Inzoli 2016a) (Figure 29). However, the
782 observations in the experiments might be covered by coalescence/break-up events of the

783 bubbles, so that these results are only a hint of the stability of the bubble column. Empirical
784 correlations for the stability of bubble columns are summarized by Besagni et al. (2018).
785

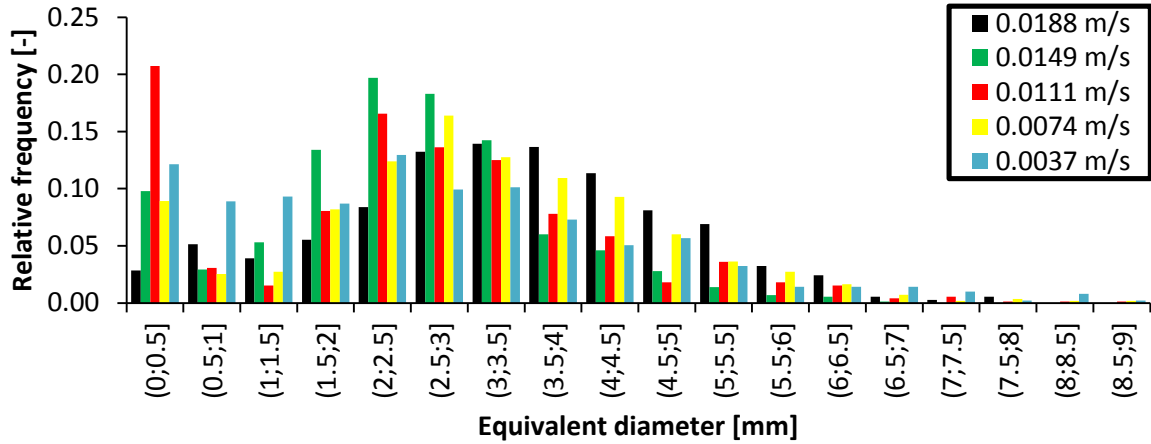


(a) Gas holdup curves

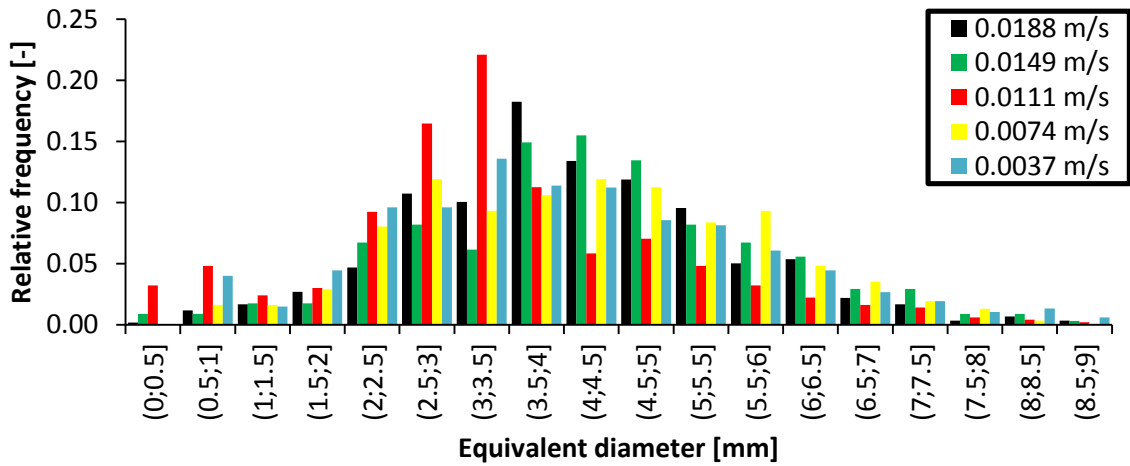
786 Figure 28 Gas holdup and flow regime transition (between the pseudo-homogenous flow
787 regime and the transition flow regime) – Data from Besagni and Inzoli (2016a)

788

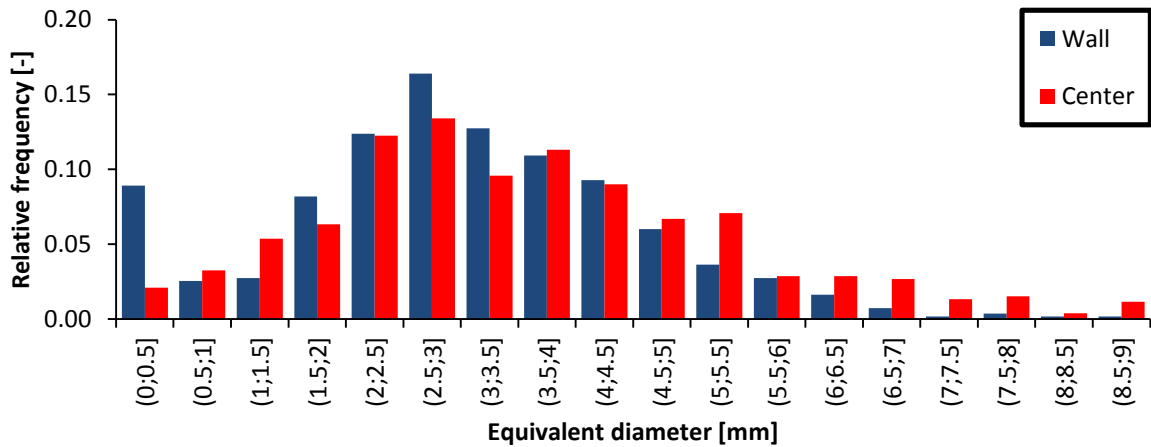
789



(a) Batch mode (measured at the center of the bubble column): influence of the superficial gas velocity

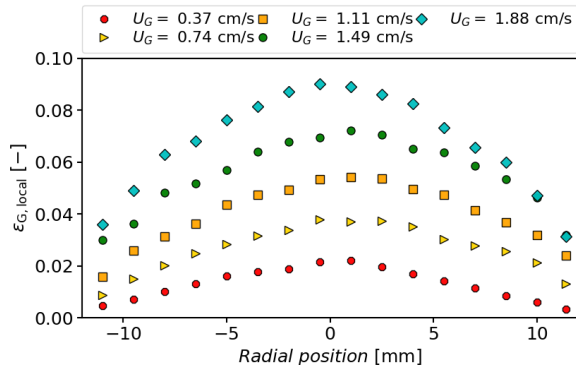


(a) Counter-current mode (measured at the center of the bubble column): influence of the superficial gas velocity.

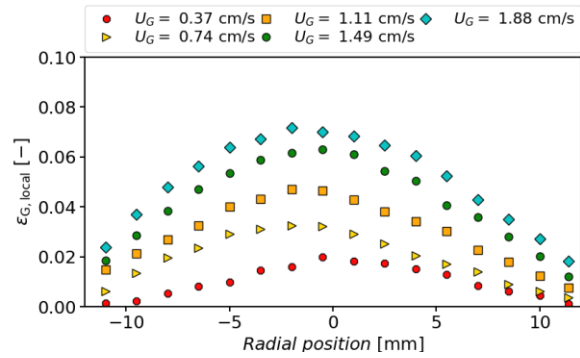


(a) Batch mode (at $U_G = 0.37 \text{ cm/s}$): comparison between measurements at the center of the column and near the wall. – Data from Besagni and Inzoli (2016a)

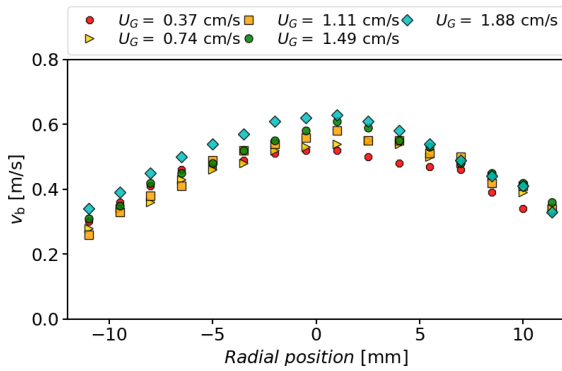
Figure 29 Bubble size distributions in the pseudo-homogeneous flow regime.



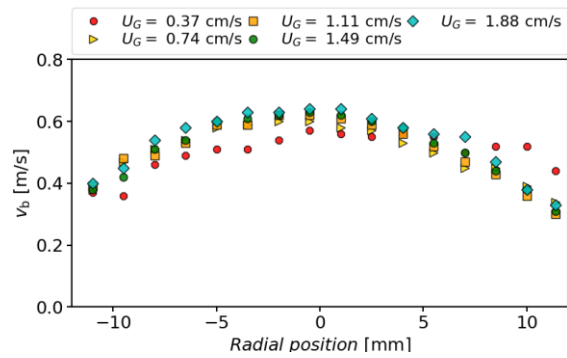
(a) void fraction profiles – 1.9 m above the gas sparger – batch mode



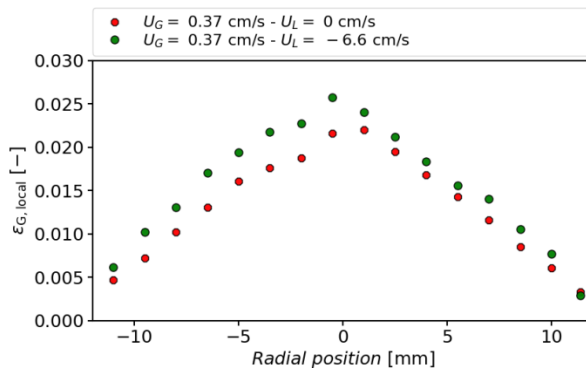
(b) void fraction profiles – 0.7 m above the gas sparger – batch mode



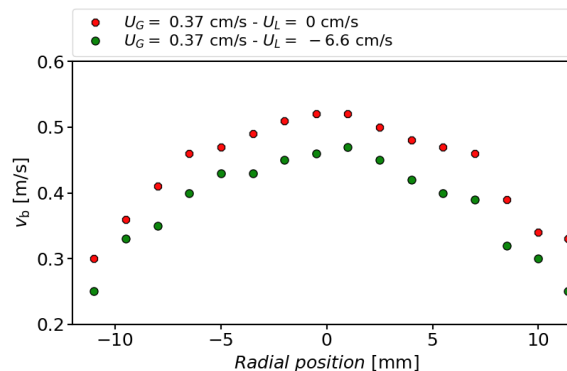
(c) bubble rising velocity – 1.9 m above the gas sparger – batch mode



(d) bubble rising velocity – 0.7 m above the gas sparger – batch mode



(e) void fraction profiles – 0.7 m above the gas sparger – influence of counter-current mode

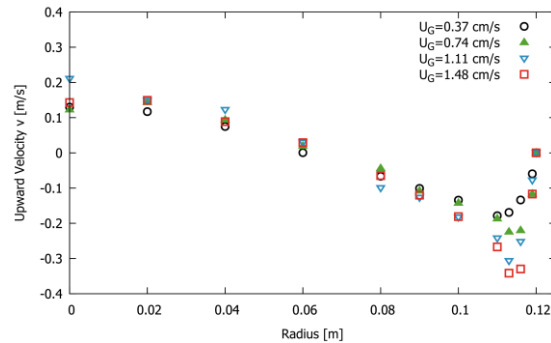
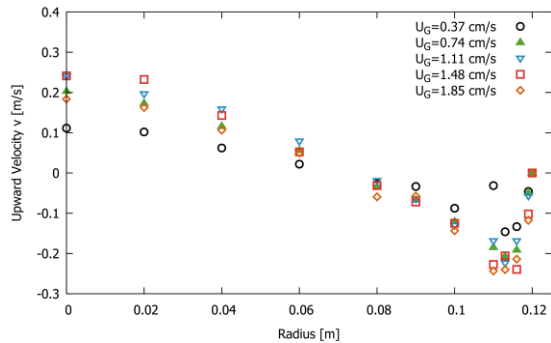


(f) bubble rising velocity – 1.9 m above the gas sparger – influence of counter-current mode

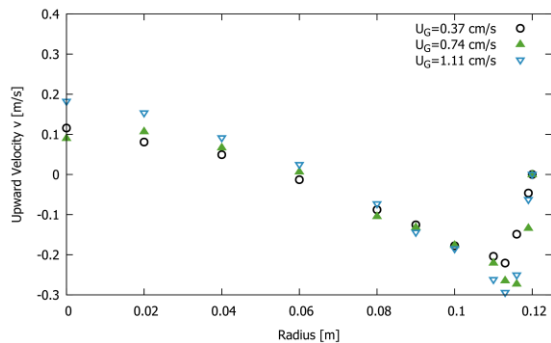
791 Figure 30 Local flow properties measured by the optical probe in the pseudo-homogenous
 792 flow regime. – Data from Besagni and Inzoli (2016a)

794 **B. Results 1.9 m above the sparger**

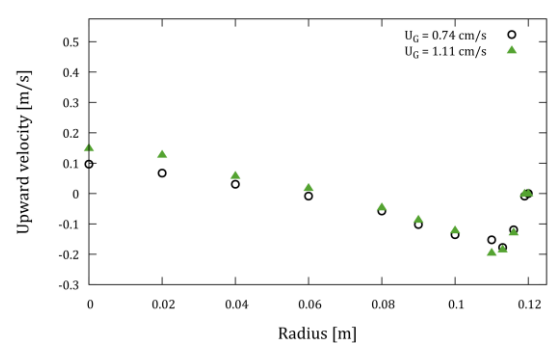
795 Since inlet effects are present at the measuring position 1.9 m above the sparger, these
 796 results were not in the focus of the main text. For completeness, the results at this
 797 measuring position are given in the following



a) Batch mode



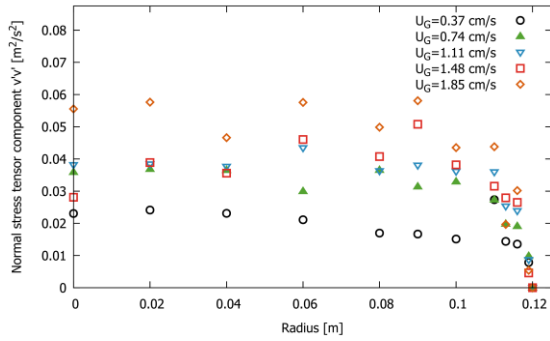
b) Superficial liquid velocity = -3.3 cm/s



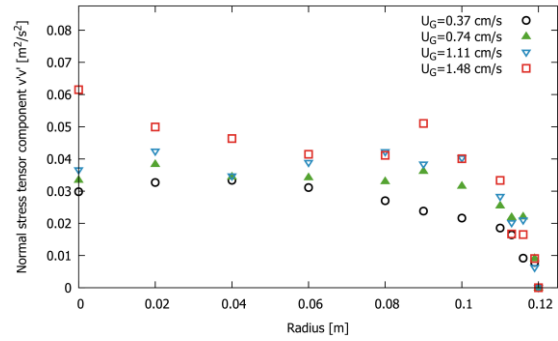
c) Superficial liquid velocity = -6.6 cm/s

d) Superficial liquid velocity = -9.2 cm/s

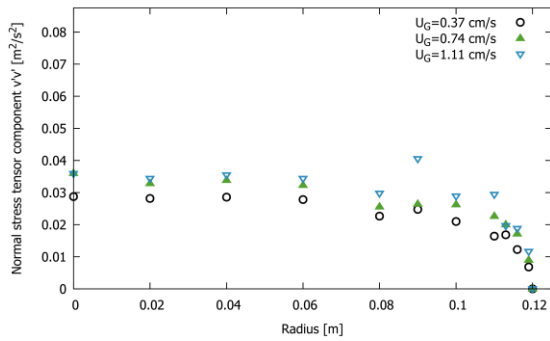
798 Figure 31 Averaged upward liquid velocities for different superficial gas velocities at
 799 different superficial liquid velocities, U_L , 1.9 m above the gas sparger.



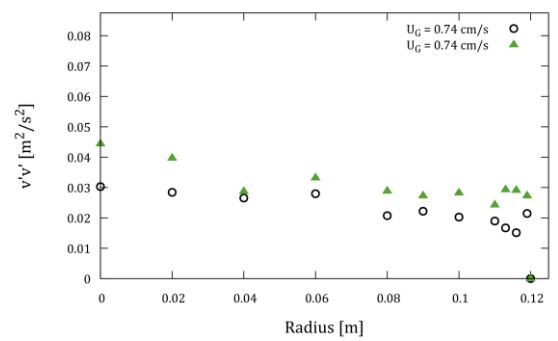
a) Batch mode



b) Superficial liquid velocity = -3.3 cm/s



c) Superficial liquid velocity = -6.6 cm/s



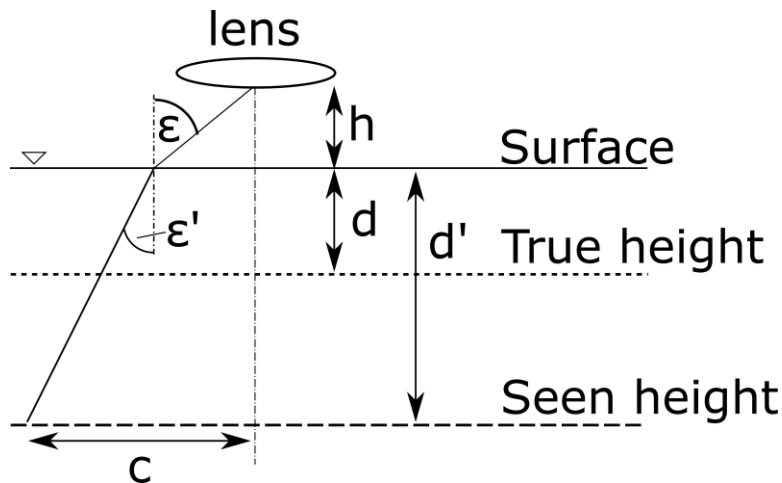
d) Superficial liquid velocity = -9.2 cm/s

800 Figure 32 Normal Reynolds stresses in upward direction for different superficial gas
 801 velocities at different counter-current flow setups 0.7 m above the gas sparger.

802 C. Optical distortion

803 Due to the different Refraction indices, an optical distortion is present. This distortion is
 804 in the following calculated based on the assumption made in Section 2.3 and as shown
 805 in Figure 33.

806

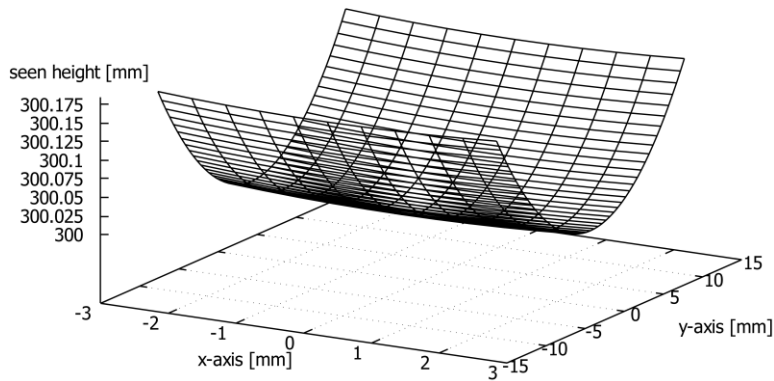


807

808

Figure 33 Calculating the distortion due to the different refracting indices.

809 Due to the different speed of light in water and Plexiglas, a light beam is refracted.
810 Therefore, the depth of field is not a plane but rather a bend surface since the light
811 refraction is a function of the distance to the surface, h , the distance from the lot, c , the focal
812 length of the camera lens, and the water depth d . However, the effect of a bended depth of
813 field is minor as shown in Figure 34, where the depth of field is shown for the measuring
814 position in the center of the column. The deviation to a flat depth of field is below 0.175
815 mm for all measuring positions; therefore, this effect can be neglected from now on.



816

817 Figure 34 Bended depth of field due to refraction in the present setup. At $x = 0$ mm and
818 $y = 0$ mm is the center of the picture.

819 7 References

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